



Lynden Garden Block Pumping Station and Forcemain Design Development

Conceptual Design Report
Final

November 8, 2023



Prepared for:
Welton & Innes Limited Partnership



November 8, 2023

RVA R226497

Welton & Innes Limited Partnership
3700 Steeles Avenue West, Suite 800
Vaughan, ON L4L 8M9

Attention: Herthana Siva
hsiva@sorbara.com

Re: Conceptual Design Report
Lynden Garden Block Pumping Station and Forcemain Design Development

Please find enclosed the Conceptual Design Report including a site plan drawing for the referenced project for your review prior to the submission to the City of Brantford.

Please do not hesitate to contact the undersigned if you have any questions.

Yours very truly,

R.V. ANDERSON ASSOCIATES LIMITED

Evan
Toews

Digitally signed by Evan Toews
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Evan Toews, P.Eng.
Project Manager

Welton & Innes Limited Partnership

Lynden Garden Block Pumping Station and Forcemain Design Development

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Final

City of Brantford

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1.0 INTRODUCTION

The Lynden Garden Block is located at 299 Lynden Road, located on the eastern most edge of the City of Brantford, west of the Canadian National Railway (CNR), north of Lynden Road. The Lynden Garden Block Pumping Station (PS) will service the Lynden Garden Block and the future East Expansion Lands located north of Highway 403 and east of Garden Avenue.



Figure 1.1 Lynden Garden PS - Key Plan

The PS will be located north of the intersection of Lynden Road and Garden Avenue in the proposed subdivision and will serve an approximate population of 18,619 persons.

This report is provided to summarize the conceptual design of the proposed PS.

2.0 DATA SOURCES

2.1 External Drawings and Documentation

The following list of drawings and documentation were referenced by RVA in the development of design parameters for the SPS:

- Lynden Garden Block Subdivision design drawings by Urbantech Consulting, dated October 2022.
- Lynden Garden Block Sanitary Sewer design sheets by Urbantech Consulting, dated 28/09/22.

- Wastewater demand data for the East Expansion Area provided by Urbantech Consulting.

2.2 Codes, Standards, & Guidelines

The following list of documents were referenced and are adhered to by RVA in the development of design parameters for the SPS:

- City of Brantford - Wastewater - Design and Construction Manual, Vertical Municipal Infrastructure Standards – January 2023
- City of Brantford - Sanitary Sewer - Design and Construction Manual, Linear Municipal Infrastructure Standards – February 2023
- Design Guidelines for Sewage Works 2008 (Ministry of Environment, Conservation & Parks)
- Hydraulic Institute Standards

3.0 ENVIRONMENTAL ASSESSMENT REQUIREMENTS

The Environmental Assessment Act (EAA), including the Municipal Engineers' Association (MEA) Municipal Class Environmental Assessment (EA) Process, prescribe that proponents consider potential environmental effects before an infrastructure project begins. We have reviewed the EA considerations for the Lynden Garden PS to determine next steps from an EA perspective. The Municipal Class EA outlines processes that proponents, such as municipalities and in some cases private entities, must follow prior to constructing infrastructure, including sewage collection systems. Under the Municipal Class EA, the Lynden Garden PS would fall under the clause 22a in Appendix 1: Project Tables, Sewage Systems – Maintenance, Operation, Distribution, Storage & Retirement:

“Establish, extend, or enlarge a sewage collection system and all necessary works to connect the system to an existing sewage outlet, where it is required as a condition of approval on a site plan, consent plan of subdivision or plan of condominium which will come into effect under the Planning Act prior to the construction of the collection system.”

As such, projects which fall under this description, such as the Lynden Garden PS, are exempt from EAA requirements, and in turn exempt from the Municipal Class EA, provided that Planning Act requirements are fulfilled. In essence, the subdivision cannot be built without the SPS and collector sewers, so they must be built to support the subdivision.

While other clauses regarding SPS's under the Municipal Class EA could be applicable to the Lynden Garden SPS, we recommend following the Planning Act for this specific site. Initiation of the Planning Act process will be included as part of the future planning development.

4.0 PROCESS DESIGN

4.1 Capacity Design Criteria

The station is sized to service a population of 18,619 persons which results in a total peak flow of 203.4 L/s per sewer design calculations and wastewater demand data provided by Urbantech Consulting. The PS services two areas, the Sorbara Land which is located in the Lynden Garden Block and the Employment Land in the East Expansion Lands. The Sorbara Land data was referenced from the flow entering the PS in the sanitary sewer design sheets while the Employment Land data was provided directly in the wastewater demand data (listed in Appendix 1). Table 4-1 below presents the design criteria for the Lynden Garden Block PS.

Table 4-1 PS Sizing Criteria

	Population	Drainage Area (ha)	Infiltration (L/s)	Sanitary Flow (L/s)	Total Flow (L/s)
Sorbara Land	2,612	45.1	13.5	25.9	39.4
Employment Land	16,007	158.3	47.5	116.5	164.00
Total	18,619	203.4	61.0	142.4	203.4

At a peak flow of 203.4 L/s, the proposed station is classified as a **Type III facility** per the City of Brantford Vertical Municipal Infrastructure Standards. Therefore, the station will consist of a total of three (3) installed pumps (two duty operating in lead-lag sequence, with one on standby) and two (2) discharge force mains (one duty and one standby).

4.2 Wet Well Sizing

Pump Station Inlet

The pumping station receives sewage from a gravity sewer at invert 203.4 m, approximately 14 m below grade. The conceptual design considers an inlet chamber within the wet well complete with isolation gates to split the flow into two separate wet well cells. As additional measures to mitigate clogging of the pumps, the City/Client may consider removable grinders mounted to the inner wall of the wet well cells.

Pump Station Configuration and Sizing

The pumping station includes a 14 m inner diameter circular shaft which contains a divided wet well and dry well. The wet well is sized to provide volume for pump operation as well as the required 1-hour emergency storage volume; whereas the dry well is allocated for dry-pit submersible pumps, facility equipment, and an access stair well. The wet well is

further split into two cells/chambers, as per MECF guidelines and the City's standard. An isolation gate is included for isolation between the two cells for any maintenance activities.

The pump configuration considers two (2) duty pumps operating in to provide the ultimate pumping capacity of 203.4 L/s and one (1) standby pump of the same model. Pump active volume, emergency storage volume, and pump operating level are shown in table below. Detailed design criteria are shown in Appendix 2.

A below grade chamber is provided to house the flowmeter and bypass connection on each of the twin forcemain.

Table 4-2 Pump Operating Level, Emergency Storage Volume, and Pump Active Volume

Parameter	Units	Value
Overflow level	m ASL	215.05
Inlet sewer invert	m ASL	203.4
High-high water level	m ASL	203.1
High water level (lag pump start)	m ASL	202.8
High water level (lag pump stop, lead pump start)	m ASL	202.2
Low water level (pump stop)	m ASL	201.9
Low-low water level	m ASL	201.7
Wet well bottom	m ASL	200.5
Wet well plan area	m ²	61.6
Lead pump active volume req'd (4 cycles/hr)	m ³	30.6
Lead pump active volume available	m ³	36.9
Lag pump active volume req'd (4 cycles/hr)	m ³	15.3
Lag pump active volume available	m ³	18.5
Emergency storage required	m ³	732.2
Emergency storage available	m ³	735.8

4.3 Pump Sizing and Selection

The Lynden SPS is designed to be a split-cell wet well / dry well pumping station with a total of three (3) dry-pit submersible pumps. One pump is connected to both of the wet well cells while the other two pumps are connected to single opposite cells, the pumps were selected to be capable of pumping the peak flow rate of at least 203.4 L/s when two are operating together.

System curves were developed using the Hazen-Williams equation for the following three (3) conditions of suction static head conditions and Hazen-Williams 'C' factors.

- Condition A: Low sewage level in the wet well, C=120
- Condition B: Median sewage level, C=130
- Condition C: High sewage level, C=140

The total dynamic head (TDH) for Condition B was used for pump selection, as per MECP guidelines. In addition, the system curve for the overflow condition was also calculated to review the pump operating condition after an overflow event. The pumps will discharge through one of two 350 mm PVCO forcemains to the downstream MH, approximately 290 m away from the pumping station. The system curves are plotted in Figure 4.1.

The system curves and duty points were used for a preliminary selection of Xylem/Flygt pumps. The Flygt NT3202 with 354 mm impeller was selected for the primary duty point. The flow of lead pump under Condition B is 142 L/s, and the combined flow of both duty pumps is 223 L/s. When operating under the overflow condition, the static head is significantly reduced. The increased pumped flow will cause the forcemain velocity to increase beyond the recommended range. Control measures can be considered at the detailed design stage to mitigate this issue.

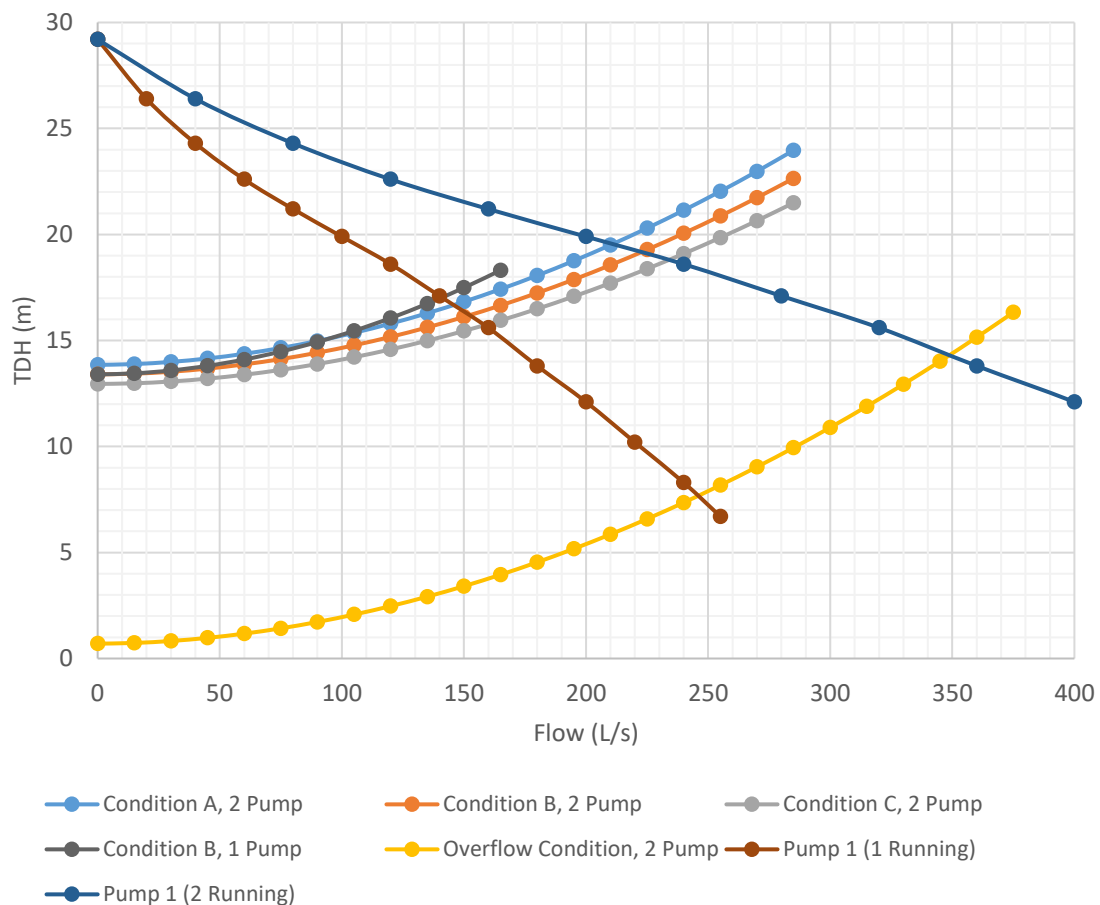


Figure 4.1 System Curves and Selected Pump Curves (Flygt NT 3202 MT 3~ 641 354mm)

The pump configuration and operating conditions are listed in Table 4.3 and detailed hydraulic design calculations are contained in Appendix 3.

Table 4.3 Pump Configuration and Operating Conditions

Parameter	Value
Peak Flow (L/s)	203.4
Pump Configuration	2 duty, 1 standby
Each Pump Capacity Req'd (L/s)	101.7
Total Dynamic Head at duty point, Condition B (m)	18.2
Selected Pump	Flygt NT 3202 MT3-641 354mm
Pump Best Efficiency Point	81.5 % at 147 L/s, 16.6 m
Motor Rated Speed (RPM)	1185
Motor Size	33 kW (44 HP)

4.4 Dry Well

The pumping station includes a 14 m inner diameter circular shaft which contains a divided wet well and dry well. The ventilated below-grade dry well will house valves and a flowmeter for each forcemain. The footprint of the dry well will approximately match that of the wet well at one-half of a 14 m diameter circular shaft. The dry well comprises a Class 1, Division 2 hazardous location per the NFPA 820 guidelines.

Process Piping, Valves, and Appurtenances

The station magnetic flowmeter, pumps, valving and appurtenances will be housed in the below ground dry well.

Forcemain(s)

Two forcemains (duty/standby) are provided, each of 350mm diameter and PVCO material (assumed White Bionax PVCO, PC235). PVC is the preferred forcemain material for the City of Brantford and is generally easier to install and repair in open cut compared to HDPE. The pipe class should be reviewed and finalized upon the completion of a Hydraulic Transient Analysis during detailed design. A motorized isolation valve for each forcemain connected to SCADA will be provided.

The forcemain alignments are from the PS wet well to the discharge maintenance hole located 300 m west of the PS on Lynden Road. The forcemains should be installed at 1.85 m depth of cover to obvert below the future road surface elevation and be continuously rising from the wet well to the discharge point, to ensure that the forcemains will drain back to the PS. If the forcemain cannot be continuously rising, then drain valve chambers should be installed at local low points and air/vacuum release valve chambers should be installed at local high points, with exact locations and valve sizing to be determined through transient analysis.

Under normal operating conditions, the duty forcemain can maintain a velocity between 1.0 m/s to 2.0 m/s, which is within the minimum and maximum acceptable velocity ranges as per the City of Brantford - Sanitary Sewer - Design and Construction Manual. If alternate pumps are selected to provide a lower minimum flow, regular flushing/swabbing is recommended to mitigate solid deposition in the forcemains. This forcemain size selection also has the ability to accommodate future development and increased future flows which could increase the operational velocity up to the maximum limit of 2.5 m/s.

4.5 Overflow

A 450mm overflow pipe is provided with invert elevation at the overflow level set 1.8 m below the Assumed Datum for Ground Elevation for the PS. During design it should be confirmed that this elevation is 0.5 m below the lowest basement flooding elevation in the wet well. The overflow is directed to the adjacent storm water management pond located in the block to the east.

4.6 Pump Station Initial Operation

At the initial stages of pump station operation, it is understood that only a fraction of the full pump station capacity would be utilized due to phased occupancy. Estimates of the initial built-out flows were developed based on design data provided by Urbantech. Assuming 10% of the ultimate population serviced and an infiltration flow equal to 40% of the peak dry weather flow, the average dry weather flow and peak wet weather flow are 5.3 L/s and 26.7 L/s, respectively. The minimum operation volume for one constant speed duty pump at 26.7 L/s incoming flow is approximately 12.9 m³ (max. 6 starts per hour), which can be met using operational changes (use of a single wet well cell and/or changing pump operating range). However, this volume would result in an exceedance of the recommended fill time as per MECP guidelines at the average flow. The reduced flow may result in excess residence time within the wet well or forcemain that can sulfides generation leading to potential for odours and corrosion. Potential mitigation strategy should be considered once initial flows are confirmed by the client.

5.0 SITE CIVIL DESIGN

The Lynden Garden Block PS (PS) pumping station will include a single-story building constructed over the wet well/dry well shaft. The above ground space of the building contains an electrical room approximately above the wet well and a process room above the dry well. The electrical room will be physically separated from the below ground wet well and dry well, and will therefore comprise an unclassified space per the NFPA 820 guidelines. The electrical room will house the electrical equipment, control panels, and ancillary building mechanical systems and equipment. The process room will contain access to the dry well and allow removal of the process equipment, and have sub-rooms for storage, washroom facilities, and odour control systems as required. The building and site layout are shown on the conceptual site plan drawing in Appendix 4.

The total footprint of the surface building containing the electrical room and process room will be approximately 14.6 x 11.5 metres, or 168.0 m² (including walls). The building is sized to provide the assumed necessary clearances for required equipment, as well as walking and standing space through the building as necessary. The process room over the dry well is sized to provide access and removal capability for the pumps, valves, flowmeters, and other process equipment.

The aesthetic quality of the building, including materials and finishes, should be designed to be coherent with existing surrounding structures.

5.1 Site Location

The PS new building is located at 299 Lynden Road, north of the intersection of Lynden Road and Garden Avenue by which there is road access. There is a street-facing main entrance, which includes a double door into the electrical room and a double door leading towards process room. A back double door towards the electrical room is adjacent to the parking area.

This site location was provided by Urbantech in the Lynden Garden Block Subdivision design drawings, see Appendix 5.

5.2 Site Access

The Lynden Garden PS is proposed to have one site access:

- 1) A single 10.0m wide driveway access to the site with 8.0m radius tie-in apron to Lynden Road.

The pumping station site will be able to accommodate a Transport - Single Unit Tanker Trailer, equivalent to a Vacuum Truck with a length of 12 meters. The site will also contain 4 standard-sized parking spaces.

The driveway access will allow vehicles to access parking, electrical room door and providing maintenance access to inlet bypass chamber, wet well and odour control unit to the side of the pumping station.

5.3 Site Sizing

The required property block for the pumping station site was sized at 45 x 45 meters. This allows sufficient space for the pumping station below ground and above ground structures, inlet chamber, and external generator and transformer, while providing room for a Transport - Single Unit Tanker Trailer to enter the site to service the station, turn-around, and exit the site. This estimate assumes that minimal site grading will be required.

5.4 Yard Piping

With respect to yard piping, we have assumed sanitary, forcemain, water and storm connections as following:

- 450mm dia. sanitary sewer to receive local sewage and convey to the half-14000mm dia. I.D. wet well;
- Twin 350mm dia. Force mains to receive sewage from the half-14000mm dia. I.D. wet well and convey out of the pumping station site;
- 150mm dia. domestic water connection;
- 450mm dia. overflow pipe connecting to the adjacent stormwater management pond located to the east.

5.5 Provisions

Influent Flow Monitoring

An inlet bypass site MH is provided immediately upstream of the station along the influent sewer, large enough to house the correct size portable bypass pumps for complete station rehabilitation, maintenance purposes, and/or complete station failure. This MH can be also used for flow monitoring purposes. It is located within the limits of the pump station property thereby not requiring traffic control in the public ROW in order to gain access.

6.0 CONCEPTUAL ELECTRICAL DESIGN

6.1 Power Supply and Distribution System

We have estimated the power supply requirements for the station based on the assumed major electrical loads on site including process equipment (pumps and grinder), HVAC equipment (fans and odour control unit), and other small electrical loads (heaters, motorized equipment, and lighting). Assuming these loads we anticipate that the service will be greater than 500kVA, 600A from the transformer based on similarly sized stations, however the exact load requirements must be determined by performing an Electrical Load Analysis during the design phase.

A new Motor Control Center (MCC) is proposed to be installed inside the electrical room in the on-site control building. The Main Circuit Breaker, Hydro Entrance (CT's and PT's), Automatic Transfer Switch (ATS), Digital Power Meter (DPM), Variable Frequency Drive (VFD) and Direct On-Line (DOL) starters for the motors and feeder breakers will be installed in the MCC. A power factor correction system, surge protective device and a lightning arrester system will be provided.

A transformer and lighting panel will be required and could be installed in the electrical room to supply power for the low voltage loads. The panel board will be equipped with transient voltage surge suppression device.

6.2 Generator

A backup power diesel generator is recommended to support the facility upon loss of Hydro supply. The pumping station site will accommodate a permanent on-site diesel standby power generator and a transformer, each mounted on separate concrete pads and protected by bollards. The proposed generator will be an outdoor generator equipped with sub-base fuel tank for aesthetic purposes. The fuel tank will be sized to provide fuel storage duration consistent with the Client/City's needs.

7.0 CONCEPTUAL CAPITAL AND OPERATING COSTS

Conceptual design level capital and operating cost estimates have been developed for the Lynden Garden Block PS based on the assumptions made in this conceptual design report. The conceptual cost estimates are very high level based on preliminary understanding of the pumping station requirements, and therefore are subject to change pending further discussion and design.

Table 7.1 Conceptual Capital Cost Estimate

Item	Cost
General Requirements, Mobilization, Environmental Protection and Controls	\$1,000,000.00
Siteworks Including Excavations, Grading, Access Roadway, Fencing, Landscaping, Stormwater Management	\$450,000.00
Wet Well/Dry Well Concrete Shaft, Substructure, Including Reinforcing, Formwork, Waterproofing	\$2,350,000.00
Electrical Building Superstructure, Including Masonry, Roofing, Doors, Windows, Thermal and Moisture Protection	\$740,000.00
Pumps (4), Process Mechanical Equipment, and Appurtenances	\$620,000.00
Miscellaneous Metal Fabrications, FRP, Wood, and Plastics	\$495,000.00
Electrical, Instrumentation and Control, SCADA	\$1,365,000.00
Building Mechanical including Outdoor Generator, Fuel Tank, and Odour Control System	\$1,110,000.00
Allowance for Station Overflow	\$100,000.00
Yard Piping Including Manholes, Sewers, and Water Servicing	\$250,000.00
Sub-total	\$8,480,000.00
Conceptual Design Contingency (25%)	\$2,120,000.00
Total Estimated Capital Cost (Not Including Applicable Taxes)	\$10,600,000.00

Table 7.2 Conceptual Operating Cost Estimate

Item	Cost
Operating and Maintenance Costs	\$52,000/year

The operating and maintenance costs are assuming a 50-year life span for the pumping station.

APPENDIX 1

Urbantech Sanitary Sewer Design Sheets and Wastewater Flow Data

SANITARY SEWER DESIGN SHEET

299 Lynden Road

City of Brantford

PROJECT DETAILS

Project No: 19-617

Date: 28-Sep-22

Designed by: Bob Moir

Checked by: Nava Pokharel, P.Eng.

DESIGN CRITERIA

Min Diameter = 250 mm

Avg. Domestic Flow = 245.0 l/c/d

Mannings 'n'= 0.013

Infiltration = 0.300 l/s/ha

Min. Velocity = 1.00 m/s

Max. Peaking Factor = 4.00

Max. Velocity = 2.50 m/s

Min. Peaking Factor= 2.00

Factor of Safety = 4 %

NOMINAL PIPE S

STREET	FROM MH	TO MH	RESIDENTIAL							COMMERCIAL/INDUSTRIAL/INSTITUTIONAL						FLOW CALCULATIONS							SLOPE (%)	PIPE DIAMETER (mm)	PIPE DATA		
			AREA (ha)	ACC. AREA (ha)	UNITS (#)	DENISTY (P/ha)	DENSITY (P/unit)	POP	ACCUM. RES. POP.	AREA (ha)	ACC. AREA (ha)	EQUIV. POP. (p/ha)	FLOW RATE (l/s/ha)	EQUIV. POP.	ACCUM. EQUIV. POP.	INFILTRATION (l/s)	TOTAL ACCUM. POP.	PEAKING FACTOR	RES. FLOW (l/s)	COMM. FLOW (l/s)	ACCUM. COMM. FLOW (l/s)	TOTAL FLOW (l/s)			FULL FLOW CAPACITY (l/s)	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY (m/s)
Street H	9A	8A	0.58	0.58	7		3.05	22	22							0.2	22	4.00	0.2			0.4	1.00	250	59.5	1.21	0.31
Street H	8A	7A	1.70	2.28	32		3.05	98	120							0.7	120	4.00	1.4			2.0	1.00	250	59.5	1.21	0.55
Street H	7A	6A	0.91	3.19	18		3.05	55	175							1.0	175	4.00	2.0			2.9	0.50	250	42.0	0.86	0.49
Street H	6A	5A	0.84	4.03	12		3.05	37	212							1.2	212	4.00	2.4			3.6	0.50	250	42.0	0.86	0.53
Street A	5A	4A	1.62	5.65	42		2.71	114	326							1.7	326	4.00	3.7			5.4	0.50	250	42.0	0.86	0.59
Street A	10A	4A	1.42	1.42	22		2.64	59	59							0.4	59	4.00	0.7			1.1	1.00	250	59.5	1.21	0.42
Street C	4A	3A	0.31	7.38	9		2.47	23	408							2.2	408	4.00	4.6			6.8	0.50	250	42.0	0.86	0.63
Street F	14A	13A	1.62	1.62	30		3.05	92	92							0.5	92	4.00	1.0			1.5	1.00	250	59.5	1.21	0.47
street E	7A	13A	0.13	2.41					120							0.7	120	4.00	1.4			2.1					
Street F	13A	12A	0.85	4.88	18		3.05	55	267							1.5	267	4.00	3.0			4.5	0.50	250	42.0	0.86	0.57
Street F	12A	11A	0.85	5.73	18		3.05	55	322							1.7	322	4.00	3.7			5.4	0.50	250	42.0	0.86	0.59
Street B	5A	11A	0.17	4.20					212							1.3	212	4.00	2.4			3.7					
Street F	11A	3A	1.43	11.36	42		2.71	114	648							3.4	648	3.91	7.2			10.6	0.50	250	42.0	0.86	0.69
Street C	3A	2A	0.37	19.11	12		2.47	30	1086							5.7	1086	3.78	11.6			17.4	0.50	250	42.0	0.86	0.80
Street M	21A	20A	0.71	0.71	9		3.05	28	28							0.2	28	4.00	0.3			0.5	1.00	250	59.5	1.21	0.31
Street E	13A	20A	0.13	4.16					212							1.2	212	4.00	2.4			3.7					
Street G	20A	19A	0.30	5.17	5		3.05	16	256							1.6	256	4.00	2.9			4.5	1.00	250	59.5	1.21	0.69
Street G	19A	18A	0.36	5.53	7		3.05	22	278							1.7	278	4.00	3.2			4.8	1.00	250	59.5	1.21	0.71
Street G	18A	17A	0.34	5.87	6		3.05	19	297							1.8	297	4.00	3.4			5.1	0.50	250	42.0	0.86	0.57
Street B	11A	17A	0.17	10.10					534							3.0	534	3.96	6.0			9.0		250			
Street G	17A	16A	0.30	16.27	5		3.05	16	847							4.9	847	3.85	9.2			14.1	0.50	250	42.0	0.86	0.75
Street G	16A	15A	0.36	16.63	7		3.05	22	869							5.0	869	3.84	9.5			14.4	0.50	250	42.0	0.86	0.75
Street G	15A	2A	0.23	16.86	4		3.05	13	882							5.1	882	3.83	9.6			14.6	0.50	250	42.0	0.86	0.77
Street C	2A	1A	1.29	37.26	57		2.47	141	2109							11.2	2109	3.57	21.3			32.5	0.50	250	42.0	0.86	0.93
Street L	30A	28A	0.88	0.88	12		3.05	37	37							0.3	37	4.00	0.4			0.7	1.00	250	59.5	1.21	0.31
Street E	29A	28A	0.37	0.37	7		3.05	22	22							0.1	22	4.00	0.2			0.4	1.00	250	59.5	1.21	0.31
Street E	28A	27A	0.81	2.06	18		3.05	55	114							0.6	114	4.00	1.3			1.9	1.00	250	59.5	1.21	0.51
Street I	31A	27A	0.48	0.48	6		3.05	19	19							0.1	19	4.00	0.2			0.4	1.00	250	59.5	1.21	0.31
Street I	27A	26A	0.13	2.67					133							0.8	133	4.00	1.5			2.3	0.50	250	42.0	0.86	0.45
Street I	26A	25A	0.13	2.80					133							0.8	133	4.00	1.5			2.3	0.50	250	42.0	0.86	0.46
Street I	25A	24A	0.14	2.94					133							0.9	133	4.00	1.5			2.4	0.50	250	42.0	0.86	0.46
Street I	24A	23A	0.17	3.11					133							0.9	133	4.00	1.5			2.4	0.50	250	42.0	0.86	0.46
Street I	23A	22A	0.16	3.27					133							1.0	133	4.00	1.5			2.5	0.50	250	42.0	0.86	0.46
Street I	22A	1A	0.11	3.38					133							1.0	133	4.00	1.5			2.5	0.50	250	42.0	0.86	0.46
Street J	32A	26A	1.45	1.45	34		3.05	104	104							0.4	104	4.00	1.2			1.6	1.00	250	59.5	1.21	0.47
Street K	33A	25A	1.45	1.45	34		3.05	104	104							0.4	104	4.00	1.2			1.6	1.00	250	59.5	1.21	0.47
Street B	34A	24A	1.58	1.58	45		2.71	122	122							0.5	122	4.00	1.4			1.9	1.00	250	59.5	1.21	0.51

STREET	FROM MH	TO MH	RESIDENTIAL							COMMERCIAL/INDUSTRIAL/INSTITUTIONAL						FLOW CALCULATIONS							PIPE DATA				
			AREA (ha)	ACC. AREA (ha)	UNITS (#)	DENISTY (P/ha)	DENSITY (P/unit)	POP	ACCUM. RES. POP.	AREA (ha)	ACC. AREA (ha)	EQUIV. POP. (p/ha)	FLOW RATE (l/s/ha)	EQUIV. POP.	ACCUM. EQUIV. POP.	INFILTRATION (l/s)	TOTAL ACCUM. POP.	PEAKING FACTOR	RES. FLOW (l/s)	COMM. FLOW (l/s)	ACCUM. COMM. FLOW (l/s)	TOTAL FLOW (l/s)	SLOPE (%)	PIPE DIAMETER (mm)	FULL FLOW CAPACITY (l/s)	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY (m/s)
Street N	35A	23A	1.46	1.46	56		2.47	139	139							0.4	139	4.00	1.6			2.0	1.00	250	59.5	1.21	0.55
Street O	36A	22A	1.26	1.26	56		2.47	139	139							0.4	139	4.00	1.6			2.0	1.00	250	59.5	1.21	0.55
Street E	38A	37A	0.67	0.67	7		3.05	22	22							0.2	22	4.00	0.2			0.5	1.00	250	59.5	1.21	0.31
Street E	37A	27A	1.58	2.25	28		3.05	86	108							0.7	108	4.00	1.2			1.9	0.50	250	42.0	0.86	0.42
Street J	38A	26A	1.26	1.26	28		3.05	86	86							0.4	86	4.00	1.0			1.4	1.00	250	59.5	1.21	0.47
Street E	38A	39A	0.32	0.32	5		3.05	16	16							0.1	16	4.00	0.2			0.3	1.00	250	59.5	1.21	0.31
Street K	42A	40A	0.74	0.74	9		3.05	28	28							0.2	28	4.00	0.3			0.5	1.00	250	59.5	1.21	0.31
Street K	40A	39A	1.08	1.82	18		3.05	55	83							0.5	83	4.00	0.9			1.5	1.00	250	59.5	1.21	0.47
Street K	39A	25A	1.25	3.39	28		3.05	86	185							1.0	185	4.00	2.1			3.1	0.50	250	42.0	0.86	0.49
Street B	42A	41A	1.05	1.05	20		3.05	61	61							0.3	61	4.00	0.7			1.0	1.00	250	59.5	1.21	0.38
Street B	41A	24A	1.33	2.38	37		2.70	100	161							0.7	161	4.00	1.8			2.5	1.00	250	59.5	1.21	0.59
Street N	45A	44A	0.52	0.52	7		3.05	22	22							0.2	22	4.00	0.2			0.4	0.50	250	42.0	0.86	0.22
Street N	44A	43A	0.60	1.12	10		3.05	31	53							0.3	53	4.00	0.6			0.9	1.00	250	59.5	1.21	0.38
Street N	43A	23A	1.22	2.34	46		2.47	114	167							0.7	167	4.00	1.9			2.6	0.50	250	42.0	0.86	0.46
Street O	47A	46A	0.49	0.49	8		3.05	25	25							0.1	25	4.00	0.3			0.4	0.50	250	42.0	0.86	0.22
Street O	PARK	46A	2.38	2.38		90		215	215							0.7	215	4.00	2.4			3.2					
Street O	46A	22A	1.20	4.07	46		2.47	114	354							1.2	354	4.00	4.0			5.2	1.00	250	59.5	1.21	0.75
Street D	COMM	1A	3.58	3.58		90		323	323							1.1	323	4.00	3.7			4.7					
Street D	1A	2B	0.88	45.10	19		2.47	47	2612							13.5	2612	3.49	25.9			39.4	0.50	250	42.0	0.86	0.97
	4B	3B																				0.30	250	32.6	0.66	0.17	
	3B	2B																				0.30	250	32.6	0.66	0.17	
	2B	1B		45.10					2612							13.5	2612	3.49	25.9			39.4	0.30	300	53.0	0.75	0.80
	1B	SPS-2		45.10					2612							13.5	2612	3.49	25.9			39.4	0.30	300	53.0	0.75	0.80
	SPS-1	5B																						250			



SIZE USED

**PERCENT
FULL
(%)**

1%
3%
7%
9%
13%
2%
16%
3%
11%
13%
25%
41%
1%
7%
8%
12%
34%
34%
35%
77%
1%
1%
3%
1%
5%
6%
6%
6%
6%
6%
3%
3%
3%

Urbantech Consulting, A Division of Leighton-Zec Ltd.
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TEL: 905.946.9461 FAX: 905.946.9595
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PERCENT FULL (%)
3%
3%
1%
5%
2%
0%
1%
3%
7%
2%
4%
1%
2%
6%
1%
9%
94%
74%
74%

Provided by Urbantech Consulting, 2023.02.15

Ultimate SPS (Block 2)

The ultimate SPS will be constructed as part Phase 2 and built for full build out conditions of the East Expansion Area which also includes Block 1. The total catchment area to the ultimate SPS will be 158.3 ha with an equivalent residential population of 3,963 persons and employment population of 12,044 persons for a total population of 16,007 persons. The resultant wastewater demands for the East Expansion Area will be:

Average Daily Dry Weather Flow	= 48.9 L/s
Peaked Dry Weather Flow	= 116.5 L/s
Infiltration Flow	= 47.5 L/s
Total Design Flow	= 164.0 L/s

APPENDIX 2

Design Criteria - Wet Well Sizing Calculations

Lynden Garden Block PS - Residential & Employment Lands

Conceptual Design Criteria

01-Nov-23

Pumping Station Conceptual Design Concept	
▪	The sanitary pumping station will have a total peak flow of 203.4 L/s
	Per the City of Brantford Vertical Municipal Infrastructure Standards for Type III facilities the station will comprise:
	• Split wet well/dry well design with dry pit submersible pumps
	• Inlet chamber with isolation gates to divert flows into each cell
	• Inlet bypass chamber large enough to house the correct size portable bypass pumps for complete station rehabilitation, maintenance purposes, and/or complete station failure
	• Wet well interconnection gate to isolate each cell for service
	• Electrical and control panels housed in a dedicated superstructure that is unclassified
	• Ventilated below-grade dry well housing valves and a flowmeter for each forcemain
	• Three pumps (at least one standby)
	• A motorized isolation valve for each forcemain connected to SCADA will be provided.
	• Ventilation duct with a permanent explosion-proof and corrosion resistant ventilation fan
▪ Per the City of Brantford Vertical Municipal Infrastructure Standards, a minimum of 1 hour emergency storage is required for the wet well. The required emergency storage capacity of the wet well will therefore need to be in the order of 732.2 m ³ .	
▪ The total volume of the wet well, including the normal operating volume and emergency storage, will be approximately 754 m ³ . The operating volume will be approximately 49 m ³ .	
▪ To meet this requirement, based on the conceptual design criteria calculations (attached), the wet well is conceptually sized as two cells, each one-quarter of a 14 metre diameter circular shaft, with a depth of approximately 16.9 metres.	
▪ This wet well would be significantly larger than required from an operational or hydraulic standpoint. A deviation from design standards would need to be requested from the City to reduce the costs of the facility (the likelihood of achieving a deviation is not known).	
▪ The wet well will be constructed of cast-in-place concrete. The wet well will comprise a Class 1, Division 1 hazardous location per the NFPA 820 guidelines.	
▪ The station magnetic flowmeter, pumps, valving and appurtenances will be housed in the below ground dry well. The footprint of the dry well will approximately match that of the wet well at one-half of a 14 metre diameter circular shaft. The dry well comprise a Class 1, Division 2 hazardous location per the NFPA 820 guidelines.	
▪ The pumping station will include a single-story building containing an electrical room constructed over the wet/dry well shaft. The above ground spaces of the electrical room will be physically separated from the below ground wet well and dry well, and will therefore comprise an unclassified space per the NFPA 820 guidelines.	
▪ The total footprint of the surface building containing the electrical room and access room to the dry well will be approximately 14.6 x 11.5 metres, or 168 m ² (including walls).	
▪ The electrical room will house the electrical equipment, control panels, and ancillary building mechanical systems and equipment.	
▪ The pumping station will be equipped with full SCADA integrated with the City of Brantford SCADA system in accordance with City of Brantford Design Standards.	
▪ The required property block for the pumping station site is 45 x 45 meters.	
▪ The pumping station site will accommodate a permanent on-site diesel standby power generator and a transformer, each mounted on separate concrete pads and protected by bollards.	
▪ The pumping station site will be able to accommodate a Transport - Single Unit Tanker Trailer, equivalent to a Vacuum Truck with a length of 12 meters. The site will also contain 4 standard size parking spaces.	

Lynden Garden Block PS - Residential & Employment Lands

Appendix A

Sanitary Pumping Station Conceptual Design Criteria

Design Flows

Average Dry Weather Flow	56.32 L/s
Peaking Factor (Harmon)	2.5284
Peak Residential Flow	142.40 L/s
Infiltration Flow	61.0
Total Peak Flow	203.40 L/s

Influent Sewer Invert Elevations

Assumed Datum for Ground Elevation	217.3 m
375ø Collector Invert	203.4 m

Pump Initial Assumptions

Flow	135.6 L/s	assumed for single pump operation
Power Draw	>50 HP	
Suction Bell Mouth Diameter	0.35 m	
Check V	1.41 m/s	HI 9.8.6: $0.6 < V < 2.7$; 1.7 m/s recommended
Minimum Submergence	0.963 m	HI 9.8; Eq. 9.8.6.3

Pumping Station Setpoint Elevations

Pumping Station Diameter	14 m ²
% PS Area as Wet Well	40%
Wet Well Plan Area	61.6 m ²
Sewer Invert	203.4 m
How Much Invert Freeboard Over HHWL?	300 mm
HHWL	203.1 m
How Much Freeboard Over HWL P2?	300 mm
HWL P2	202.8 m
How Much Freeboard Over HWL P1?	300 mm
HWL P1	202.5 m
How Much Operating Range?	600 mm
LWL	201.9 m
How Much Freeboard Over LLWL?	200 mm
LLWL	201.7 m
Allowance for Suction Inlet?	1000 mm
Suction Inlet	200.7 m
Suction Inlet Clearance	200 mm
Floor of Station	200.5 m
Elevation of Top of Wet Well Cover?	217.3 m
Depth of Wet Well	16.8 m

Pump Cycle Time For Ultimate Build-out Development

Safety Factor for Capacity vs. Peak Flow	0 %	
Target Starts per Hour	4	if <50HP, max 6 starts, if >50 HP, max 4 starts
Cycle Time	900 s	
Pump Capacity (1 Pump Operation)	135.60 L/s	
Operating Volume 1	36.95 m ³	
Incoming Flow (Q _{in,1})	67.8 L/s	min cycle time when Q _{in} = 0.5 Q _{p1}
Required Operation Vol1	30510 L	per HI 9.7 Eq. B.2
	30.5 m ³	
Operating Vol 1 > Req'd?	TRUE	
Operating Volume 2	18.47 m ³	
Pump Capacity (2 Pump Operation)	203.40 L/s	
Incoming Flow (Q _{in,2})	169.5 L/s	min cycle time when Q _{in} = 0.5 (Q _{p1} +Q _{p2})
Required Operation Vol2	15255.0 L	
	15.3 m ³	
Operating Vol 2 > Req'd?	TRUE	
Fill Time @ Average Flow	10.93 min	

Lynden Garden Block PS - Residential & Employment Lands

Appendix A

Sanitary Pumping Station Conceptual Design Criteria

Emergency Wet Well Storage Volume

Overflow Pipe Size	450 mm
Overflow Elevation (estimated)	215.05 m
Alarm Level (HHWL)	203.1 m
Wet Well Emergency Storage Capacity (Ref: HHWL)	735.82 m ³
Pump Start Level (HWL)	202.80 m
Total Capacity for Wet Well Emergency Storage (Ref: HWL)	754.30 m ³

Emergency Storage for Ultimate Development

Emergency Storage Volume Wet Well	735.82 m ³
Minutes of Emergency Storage in System	60.29 minutes
Hours of Emergency Storage in System	1.00 hours

Forcemain to Discharge

Length	288.6 m	
Elevation Leaving Wet Well	201.7 m	
Discharge Elevation	215.75 m	
Q pump	135.60 L/s	
Nominal ID of Forcemain	364 mm	White Bionax PVCO, PC235, Nom. 350mm pipe
Velocity at Pump Capacity	1.3031 m/s	
Pipe Area	0.104 m ²	
Pipe Volume	30.03 m ³	
Ratio of Useable Storable to Pipe Volume	81.29%	
Forcemain Residence Time	12.19 min	

APPENDIX 3

Hydraulic Design Calculations

Lynden Garden Block PS

Total Capacity of the System would be determined by:

Two duty one standby pump. Lead-lag operation

Pump Station Flow Requirements				
Flows				
Design Rate	203.4 L/s	17574	m3/day	203.4 L/s
Firm Capacity	203.4 L/s	17574	m3/day	203.4 L/s
No. Duty Pumps		2	No.	
Flow per Pump		8787	m3/day	101.7 L/s
No. Standby pumps		1	No.	
Total Pumps		3		

Lynden Garden Block PS

Design Philosophy							
-Flow from WW to discharge MH							
Hydraulic Profile Summary							
Common discharge line ID						0.3640	m
Discharge line length						289	m
Max Discharge Pipe Velocity						1.95	m/s
Sump Low Water Level Elevation						201.90	Elv. (m)
Sump High Water Level Elevation						202.80	Elv. (m)
Elevation of Pump Impeller Centre Line						201.60	Elv. (m)
Pump Station Ground Level (m)						200.80	Elv. (m)
Max Discharge Elevation HWL (m)						215.75	Elv. (m)
Max Discharge Elevation LWL (m)						215.75	Elv. (m)
Vapour Pressure at t=25°C						0.32	m
Atmospheric Pressure						10.09	m
Partial pressure of dissolved gasses (Volatile organic matter in waste water =0.6m)						0.60	m
NPSH Available						9.47	m

Air pressure above sea level can be calculated as

$$p = 101325 (1 - 2.25577 \cdot 10^{-5} h)^{5.25588} \tag{1}$$

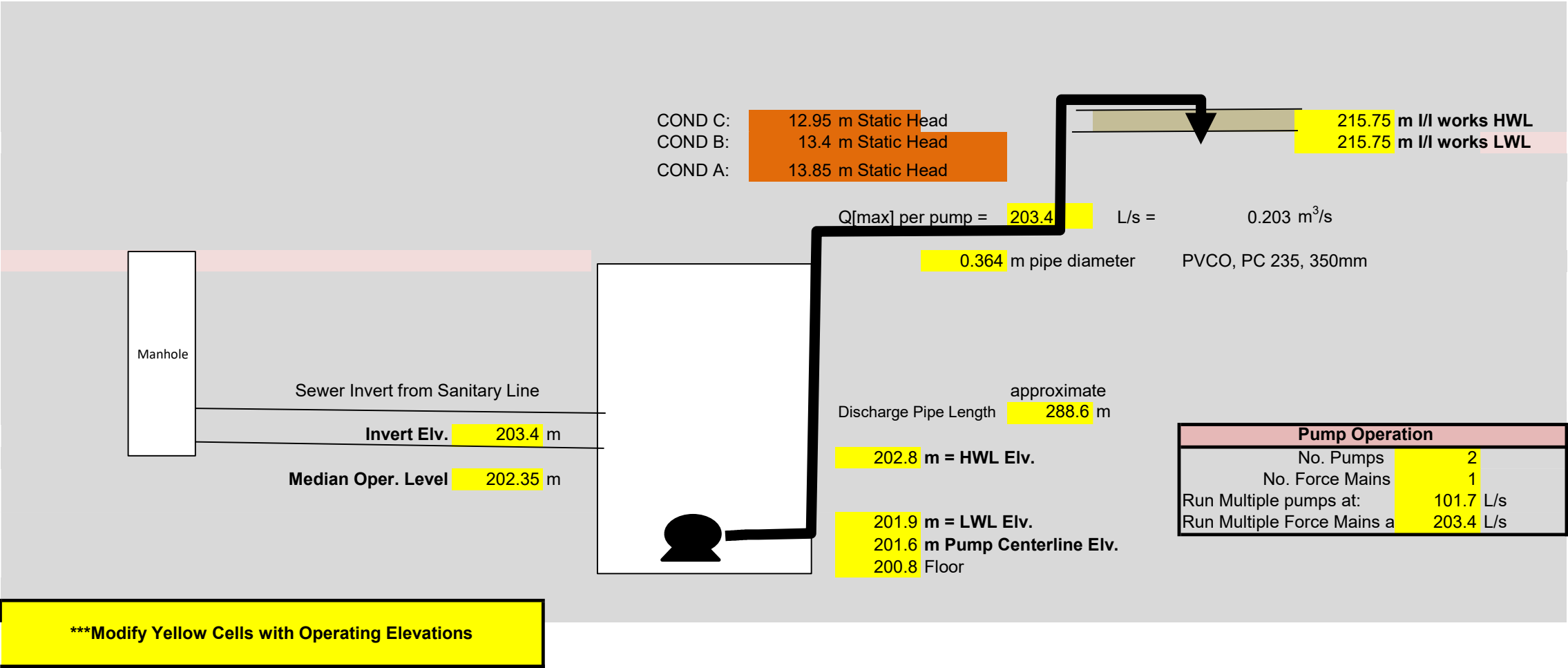
where

101325 = normal temperature and pressure at sea level (Pa)

p = air pressure (Pa)

h = altitude above sea level (m)

Hydraulic Profile



SUMMARY		Condition A: C = 120
Common discharge line ID (m)		0.364
Common discharge line Length (m)		288.6
Max Velocity (m/s)		1.95
Conditiona A/B/C Operation Level		201.90
Elevation of Pump Impeller Centre Line		201.60
Pumping Station Ground Level (m)		200.80
Discharge Elevation (m) (Tank Level)		215.75
Vapour Pressure at t=25°C (m)		0.32
Atmospheric Pressure (m)		10.09
Partial pressure of dissolved gasses (Volatile organic matter in waste water =0.6m)		0.600
Factor of Safety		1.000
NPSH Available (m)		8.20
Pump Flow at Best Efficiency Point (BEP) (m³/s)		0.083
Preferred Operating Region-Low Limit (70% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.058
Preferred Operating Region-High Limit (120% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.100
Operating Conditions Summary		

Design Flow: 0.2034 m³/s

Standard Flow Conditions

Conditions: Condition A: C = 120

Project Lynden Garden Block PS

TOTAL DYNAMIC HEAD CALCULATIONS

CONDITION: A

C= 120

FLOW : start - 0.000 (m³/s)

increase increment - 0.015 (m³/s)

Roughness Coeff (SS)		120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
Pump Flow (L/s)		0	15	30	45	60	75	90	105	120	135	150	165	180	195	210	225	240	255	270	285
Pump Flow (m³/s)		0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285
Total Pumping Station Piping Friction Losses (m)		0.00	0.03	0.10	0.21	0.35	0.54	0.75	1.00	1.28	1.59	1.93	2.31	2.71	3.15	3.61	4.10	4.62	5.17	5.75	6.35
Total Pumping Station Fitting Losses (m)		0.00	0.01	0.04	0.09	0.17	0.26	0.38	0.51	0.67	0.85	1.04	1.26	1.50	1.76	2.05	2.35	2.67	3.02	3.38	3.77
Static Head (m)		13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85	13.85
Total Dynamic Head Including PS Losses (m)		13.85	13.89	13.99	14.15	14.37	14.65	14.98	15.36	15.80	16.29	16.83	17.42	18.06	18.76	19.50	20.30	21.14	22.03	22.98	23.97
	(ft)	45.44	45.56	45.90	46.43	47.15	48.05	49.14	50.40	51.83	53.44	55.21	57.16	59.27	61.54	63.99	66.59	69.36	72.29	75.38	78.64

FLOW THROUGH SECTIONS: (m³/s)			Multiple Pumps/For ce Mains	Flow Through Pipe Sections (L/s)																		
Sec 1: Suction		2	0.000	0.008	0.015	0.023	0.030	0.038	0.045	0.053	0.060	0.068	0.075	0.083	0.090	0.098	0.105	0.113	0.120	0.128	0.135	0.143
Sec 2: Discharge Piping		2	0.000	0.008	0.015	0.023	0.030	0.038	0.045	0.053	0.060	0.068	0.075	0.083	0.090	0.098	0.105	0.113	0.120	0.128	0.135	0.143
Sec 3: Forcemain		1	0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285

HEAD LOSS THROUGH PIPE [Hazen-Williams formula for Metric Units h=L *{V/0.85°C*(D/4)^{0.63}}^{1/0.54}]

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Pipe Material	Pipe Sectional Area (m ²)	V=Q/A (m/s) (Max)		Pipe Length (m)		HEAD LOSS (M) THROUGH PIPE																								
Section 1: Pumping Station Suction Line																																	
Section 1	300	0.3147	S.S.	0.078	1.31		5.00		0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.04	0.04	0.05	0.05	0.06					
Section 2: Pumping Station Discharge Line																																	
Section 2	300	0.3147	S.S.	0.078	1.31		40.00		0.00	0.00	0.01	0.01	0.03	0.04	0.05	0.07	0.09	0.11	0.14	0.17	0.19	0.23	0.26	0.29	0.33	0.37	0.41	0.45					
Section 3: Common Discharge/Forcemain																																	
Section 3	350	0.3640	PVC	0.104	1.96		289.00		0.00	0.03	0.09	0.19	0.33	0.49	0.69	0.92	1.18	1.46	1.78	2.12	2.49	2.89	3.32	3.77	4.25	4.75	5.28	5.84					
TOTAL HEADLOSS THROUGH Piping										0.00	0.03	0.10	0.21	0.35	0.54	0.75	1.00	1.28	1.59	1.93	2.31	2.71	3.15	3.61	4.10	4.62	5.17	5.75	6.35				
TOTAL HEADLOSS THROUGH Piping For Sludge (m) with average multiplication factor 1% sludge or below = water										0.00	0.03	0.10	0.21	0.35	0.54	0.75	1.00	1.28	1.59	1.93	2.31	2.71	3.15	3.61	4.10	4.62	5.17	5.75	6.35				

HEAD LOSS FOR PIPE FITTINGS [for Metric Units h_f=K(v²/2g)], based on Table B-6 of "Pumping Station Design", Second Edition, Butterworth Heinemann.

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Increaser Smaller ID (m)	Pipe Fitting		K-Factor	K Correction Factor	HEAD LOSS (M) THROUGH FITTINGS																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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SUMMARY		Condition A: C = 140
Common discharge line ID (m)		0.364
Common discharge line Length (m)		288.6
Max Velocity (m/s)		1.95
Conditiona A/B/C Operation Level		202.80
Elevation of Pump Impeller Centre Line		201.60
Pumping Station Ground Level (m)		200.80
Discharge Elevation (m) (Tank Level)		215.75
Vapour Pressure at t=25°C (m)		0.32
Atmospheric Pressure (m)		10.09
Partial pressure of dissolved gasses (Volatile organic matter in waste water =0.6m)		0.600
Factor of Safety		1.000
NPSH Available (m)		9.12
Pump Flow at Best Efficiency Point (BEP) (m³/s)		0.083
Preferred Operating Region-Low Limit (70% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.058
Preferred Operating Region-High Limit (120% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.100
Operating Conditions Summary		

Design Flow: 0.2034 m³/s

Standard Flow Conditions

Conditions: Condition A: C = 140Project Lynden Garden Block PS

TOTAL DYNAMIC HEAD CALCULATIONS

CONDITION: A

C= 140

FLOW : start - 0.000 (m³/s)

increase increment - 0.015 (m³/s)

Roughness Coeff (SS)		140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140	140
Pump Flow (L/s)		0	15	30	45	60	75	90	105	120	135	150	165	180	195	210	225	240	255	270	285	
Pump Flow (m³/s)		0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285	
Total Pumping Station Piping Friction Losses (m)		0.00	0.02	0.07	0.16	0.27	0.40	0.56	0.75	0.96	1.20	1.45	1.74	2.04	2.36	2.71	3.08	3.47	3.89	4.32	4.77	
Total Pumping Station Fitting Losses (m)		0.00	0.01	0.04	0.09	0.17	0.26	0.38	0.51	0.67	0.85	1.04	1.26	1.50	1.76	2.05	2.35	2.67	3.02	3.38	3.77	
Static Head (m)		12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	12.95	
Total Dynamic Head Including PS Losses (m)		12.95	12.98	13.07	13.20	13.38	13.61	13.89	14.21	14.58	14.99	15.45	15.95	16.49	17.08	17.71	18.38	19.09	19.85	20.65	21.49	
	(ft)	42.49	42.59	42.87	43.31	43.91	44.66	45.57	46.63	47.83	49.19	50.68	52.32	54.10	56.03	58.09	60.30	62.64	65.13	67.75	70.51	

FLOW THROUGH SECTIONS: (m³/s)			Multiple Pumps/For ce Mains	Flow Through Pipe Sections (L/s)																		
Sec 1: Suction		2	0.000	0.008	0.015	0.023	0.030	0.038	0.045	0.053	0.060	0.068	0.075	0.083	0.090	0.098	0.105	0.113	0.120	0.128	0.135	0.143
Sec 2: Discharge Piping		2	0.000	0.008	0.015	0.023	0.030	0.038	0.045	0.053	0.060	0.068	0.075	0.083	0.090	0.098	0.105	0.113	0.120	0.128	0.135	0.143
Sec 3: Forcemain		1	0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285

HEAD LOSS THROUGH PIPE [Hazen-Williams formula for Metric Units h=L *{V/0.85°C*(D/4)^{0.63}}^{1/0.54}]

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Pipe Material	Pipe Sectional Area (m ²)	V=Q/A (m/s) (Max)		Pipe Length (m)		HEAD LOSS (M) THROUGH PIPE																							
Section 1: Pumping Station Suction Line																																
Section 1	300	0.3147	S.S.	0.078	1.31		5.00		0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	0.04	0.04					
Section 2: Pumping Station Discharge Line																																
Section 2	300	0.3147	S.S.	0.078	1.31		40.00		0.00	0.00	0.01	0.01	0.02	0.03	0.04	0.05	0.07	0.09	0.10	0.12	0.15	0.17	0.19	0.22	0.25	0.28	0.31	0.34				
Section 3: Common Discharge/Forcemain																																
Section 3	350	0.3640	PVC	0.104	1.96		289.00		0.00	0.02	0.07	0.14	0.25	0.37	0.52	0.69	0.88	1.10	1.34	1.60	1.87	2.17	2.49	2.83	3.19	3.57	3.97	4.39				
TOTAL HEADLOSS THROUGH Piping										0.00	0.02	0.07	0.16	0.27	0.40	0.56	0.75	0.96	1.20	1.45	1.74	2.04	2.36	2.71	3.08	3.47	3.89	4.32	4.77			
TOTAL HEADLOSS THROUGH Piping For Sludge (m) with average multiplication factor 1% sludge or below = water										0.00	0.02	0.07	0.16	0.27	0.40	0.56	0.75	0.96	1.20	1.45	1.74	2.04	2.36	2.71	3.08	3.47	3.89	4.32	4.77			

HEAD LOSS FOR PIPE FITTINGS [for Metric Units h_f=K(v²/2g)], based on Table B-6 of "Pumping Station Design", Second Edition, Butterworth Heinemann.

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Increaser Smaller ID (m)	Pipe Fitting		K-Factor	K Correction Factor	HEAD LOSS (M) THROUGH FITTINGS																			
				Type	No.																						
Section 1: Pump Suction																											
	350	0.3460		Entry, sq. mouth	1	0.5	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.04	0.04	0.05	0.05	0.06
	300	0.3147		Reducer	1	0.03	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	
	300	0.3147		KGv	1	0.2	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	
	300	0.3147		Wye	1	1	1.00	0.00	0.00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09	0.11	0.12	0.14	0.15	0.17
	300	0.3147		45 Bend	1	0.2	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	
	250	0.2647		Reducer	1	0.03	1.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
	250	0.2647		90 Bend	1	0.25	1.10	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03	0.03	0.04	0.04	0.05	0.06	0.07	0.08	0.08	0.09
Section 2: Pump Discharge																											
	300	0.3150	0.2647	Increaser	1		1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	0.04	0.04	
	300	0.3147		Swing Check	1	2.5	1.00	0.00	0.00	0.00	0.01	0.02	0.03	0.04	0.06	0.08	0.10	0.12	0.14	0.17	0.20	0.23	0.27	0.30	0.34	0.38	0.43
	300	0.3147		KGv	1	0.2	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	
	300	0.3147		90 Bend	1	0.25	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	0.04	0.04
	300	0.3147		Tee, branch to line	1	1.5	1.00	0.00	0.00	0.00	0.01	0.01	0.02	0.03	0.03	0.05	0.06	0.07	0.09	0.10	0.12	0.14	0.16	0.18	0.21	0.23	0.26
	350	0.3673	0.3147	Increaser	1		1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	
Section 3: Forcemain																											
	350	0.3460		Tee, run	1	0.6	1.00	0.00	0.00	0.00	0.01	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.09	0.11	0.13	0.15	0.18	0.20	0.23	0.25	0.28
	350	0.3460		90 Bend	2	0.25	1.00	0.00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.04	0.05	0.06	0.08	0.09	0.11	0.13	0.15	0.17	0.19	0.21	0.23
	350	0.3460		Tee, turn	1	1	1.00	0.00	0.00	0.01	0.01	0.02	0.03	0.05	0.06	0.08	0.11	0.13	0.16	0.19	0.22	0.25	0.29	0.33	0.38	0.42	0.47
	350	0.3460		KGv	1	0.2	1.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03	0.03	0.04	0.04	0.05	0.06	0.07	0.08	0.08	0.09
	350	0.3460		Magflow	1	1	1.00	0.00	0.00	0.01	0.01	0.02	0.03	0.05	0.06	0.08	0.11	0.13	0.16	0.19	0.22	0.25	0.29	0.33	0.38	0.42	0.47
	350	0.3460		Tee, run	1	0.6	1.00	0.00	0.00	0.00	0.01	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.09	0.11	0.13	0.15	0.18	0.20	0.23	0.25	0.28
	350	0.3460		KGv	1	0.2	1.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03	0.03	0.04	0.04	0.05	0.06	0.07	0.08	0.08	0.09
	350	0.3640		45 bends	3	0.2	1.00	0.00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.04	0.05	0.06	0.08	0.09	0.11	0.12	0.14	0.16	0.18	0.21	0.23
	350	0.3640		Exit	1	1	1.00	0.00	0.00	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.09	0.11	0.13	0.15	0.18	0.21	0.24	0.27	0.31	0.34	0.38
Total Pipe Fitting Head Loss								0.00	0.01	0.04	0.09	0.17	0.26	0.38	0.51	0.67	0.85	1.04	1.26	1.50	1.76	2.05	2.35	2.67	3.02	3.38	3.77

SUMMARY		Condition B: C = 130
Common discharge line ID (m)		0.364
Common discharge line Length (m)		288.6
Max Velocity (m/s)		1.95
Conditiona A/B/C Operation Level		202.35
Elevation of Pump Impeller Centre Line		201.60
Pumping Station Ground Level (m)		200.80
Discharge Elevation (m) (Tank Level)		215.75
Vapour Pressure at t=25°C (m)		0.32
Atmospheric Pressure (m)		10.09
Partial pressure of dissolved gasses (Volatile organic matter in waste water =0.6m)		0.600
Factor of Safety		1.000
NPSH Available (m)		7.89
Pump Flow at Best Efficiency Point (BEP) (m³/s)		0.083
Preferred Operating Region-Low Limit (70% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.058
Preferred Operating Region-High Limit (120% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.100
Operating Conditions Summary		

Design Flow: 0.2034 m³/s

Standard Flow Conditions

Conditions: Condition B: C = 130Project Lynden Garden Block PS

TOTAL DYNAMIC HEAD CALCULATIONSCONDITION: B C= 130 FLOW : start - 0.000 (m³/s) increase increment - 0.015 (m³/s)

Roughness Coeff (SS)		130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130
Pump Flow (L/s)		0	15	30	45	60	75	90	105	120	135	150	165	180	195	210	225	240	255	270	285	
Pump Flow (m³/s)		0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285	
Total Pumping Station Piping Friction Losses (m)		0.00	0.03	0.10	0.22	0.37	0.56	0.78	1.04	1.34	1.66	2.02	2.41	2.83	3.28	3.77	4.28	4.82	5.39	6.00	6.63	
Total Pumping Station Fitting Losses (m)		0.00	0.02	0.08	0.19	0.33	0.52	0.74	1.01	1.32	1.68	2.07	2.50	2.98	3.50	4.05	4.65	5.30	5.98	6.70	7.47	
Static Head (m)		13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	13.40	
Total Dynamic Head Including PS Losses (m)		13.40	13.45	13.59	13.80	14.10	14.48	14.93	15.46	16.06	16.74	17.49	18.31	19.21	20.18	21.22	22.33	23.52	24.77	26.10	27.49	
	(ft)	43.96	44.12	44.57	45.29	46.26	47.50	48.98	50.71	52.69	54.91	57.37	60.08	63.02	66.20	69.62	73.27	77.15	81.27	85.62	90.21	

FLOW THROUGH SECTIONS: (m³/s)		Multiple Pumps/For ce Mains	Flow Through Pipe Sections (L/s)																			
Sec 1: Suction	1	0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285	
Sec 2: Discharge Piping	1	0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285	
Sec 3: Forcemain	1	0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285	

HEAD LOSS THROUGH PIPE [Hazen-Williams formula for Metric Units h=L *{V/0.85°C*(D/4)^{0.63}}^{1/0.54}]

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Pipe Material	Pipe Sectional Area (m ²)	V=Q/A (m/s) (Max)		Pipe Length (m)		HEAD LOSS (M) THROUGH PIPE																									
Section 1: Pumping Station Suction Line																																		
Section 1	300	0.3147	S.S.	0.078	2.62		5.00		0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.03	0.04	0.04	0.05	0.06	0.08	0.09	0.10	0.11	0.13	0.14	0.16	0.18						
Section 2: Pumping Station Discharge Line																																		
Section 2	300	0.3147	S.S.	0.078	2.62		40.00		0.00	0.01	0.02	0.05	0.08	0.12	0.17	0.22	0.29	0.35	0.43	0.51	0.60	0.70	0.80	0.91	1.03	1.15	1.28	1.42						
Section 3: Common Discharge/Forcemain																																		
Section 3	350	0.3640	PVC	0.104	1.96		289.00		0.00	0.02	0.08	0.17	0.28	0.42	0.60	0.79	1.01	1.26	1.53	1.83	2.15	2.49	2.86	3.25	3.66	4.10	4.56	5.04						
TOTAL HEADLOSS THROUGH Piping										0.00	0.03	0.10	0.22	0.37	0.56	0.78	1.04	1.34	1.66	2.02	2.41	2.83	3.28	3.77	4.28	4.82	5.39	6.00	6.63					
TOTAL HEADLOSS THROUGH Piping For Sludge (m) with average multiplication factor 1% sludge or below = water										0.00	0.03	0.10	0.22	0.37	0.56	0.78	1.04	1.34	1.66	2.02	2.41	2.83	3.28	3.77	4.28	4.82	5.39	6.00	6.63					

HEAD LOSS FOR PIPE FITTINGS [for Metric Units h_f=K(v²/2g)], based on Table B-6 of "Pumping Station Design", Second Edition, Butterworth Heinemann.

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Increaser Smaller ID (m)	Pipe Fitting		K-Factor	K Correction Factor	HEAD LOSS (M) THROUGH FITTINGS																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
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SUMMARY		Condition B: C = 130
Common discharge line ID (m)		0.364
Common discharge line Length (m)		288.6
Max Velocity (m/s)		1.95
Conditiona A/B/C Operation Level		215.05
Elevation of Pump Impeller Centre Line		201.60
Pumping Station Ground Level (m)		200.80
Discharge Elevation (m) (Tank Level)		215.75
Vapour Pressure at t=25°C (m)		0.32
Atmospheric Pressure (m)		10.09
Partial pressure of dissolved gasses (Volatile organic matter in waste water =0.6m)		0.600
Factor of Safety		1.000
NPSH Available (m)		21.36
Pump Flow at Best Efficiency Point (BEP) (m³/s)		0.083
Preferred Operating Region-Low Limit (70% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.058
Preferred Operating Region-High Limit (120% of BEP) of (ANSI/HI 9.6.3-1997) (m³/s)		0.100
Operating Conditions Summary		

Design Flow: 0.2034 m³/s

Standard Flow Conditions

Conditions: Condition B: C = 130

Project Lynden Garden Block PS

TOTAL DYNAMIC HEAD CALCULATIONS

CONDITION: B

C= 130

FLOW : start - 0.000 (m³/s)

increase increment - 0.015 (m³/s)

Roughness Coeff (SS)		130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130
Pump Flow (L/s)		0	15	30	45	60	75	90	105	120	135	150	165	180	195	210	225	240	255	270	285	
Pump Flow (m³/s)		0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285	
Total Pumping Station Piping Friction Losses (m)		0.00	0.02	0.08	0.18	0.31	0.46	0.65	0.86	1.10	1.37	1.67	1.99	2.34	2.71	3.11	3.54	3.98	4.46	4.95	5.48	
Total Pumping Station Fitting Losses (m)		0.00	0.01	0.04	0.09	0.17	0.26	0.38	0.51	0.67	0.85	1.04	1.26	1.50	1.76	2.05	2.35	2.67	3.02	3.38	3.77	
Static Head (m)		0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	0.70	
Total Dynamic Head Including PS Losses (m)		0.70	0.73	0.83	0.97	1.17	1.42	1.72	2.07	2.47	2.92	3.41	3.95	4.54	5.18	5.86	6.58	7.35	8.17	9.04	9.94	
	(ft)	2.30	2.41	2.71	3.19	3.85	4.67	5.65	6.80	8.11	9.57	11.19	12.97	14.90	16.98	19.21	21.60	24.13	26.81	29.64	32.62	

FLOW THROUGH SECTIONS: (m³/s)			Multiple Pumps/For ce Mains	Flow Through Pipe Sections (L/s)																		
Sec 1: Suction		2	0.000	0.008	0.015	0.023	0.030	0.038	0.045	0.053	0.060	0.068	0.075	0.083	0.090	0.098	0.105	0.113	0.120	0.128	0.135	0.143
Sec 2: Discharge Piping		2	0.000	0.008	0.015	0.023	0.030	0.038	0.045	0.053	0.060	0.068	0.075	0.083	0.090	0.098	0.105	0.113	0.120	0.128	0.135	0.143
Sec 3: Forcemain		1	0.000	0.015	0.030	0.045	0.060	0.075	0.090	0.105	0.120	0.135	0.150	0.165	0.180	0.195	0.210	0.225	0.240	0.255	0.270	0.285

HEAD LOSS THROUGH PIPE [Hazen-Williams formula for Metric Units h=L *{V/0.85°C*(D/4)^{0.63}}^{1/0.54}]

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Pipe Material	Pipe Sectional Area (m ²)	V=Q/A (m/s) (Max)		Pipe Length (m)		HEAD LOSS (M) THROUGH PIPE																									
Section 1: Pumping Station Suction Line																																		
Section 1	300	0.3147	S.S.	0.078	1.31		5.00		0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.04	0.04	0.04	0.05						
Section 2: Pumping Station Discharge Line																																		
Section 2	300	0.3147	S.S.	0.078	1.31		40.00		0.00	0.00	0.01	0.01	0.02	0.03	0.05	0.06	0.08	0.10	0.12	0.14	0.17	0.19	0.22	0.25	0.29	0.32	0.35	0.39						
Section 3: Common Discharge/Forcemain																																		
Section 3	350	0.3640	PVC	0.104	1.96		289.00		0.00	0.02	0.08	0.17	0.28	0.42	0.60	0.79	1.01	1.26	1.53	1.83	2.15	2.49	2.86	3.25	3.66	4.10	4.56	5.04						
TOTAL HEADLOSS THROUGH Piping										0.00	0.02	0.08	0.18	0.31	0.46	0.65	0.86	1.10	1.37	1.67	1.99	2.34	2.71	3.11	3.54	3.98	4.46	4.95	5.48					
TOTAL HEADLOSS THROUGH Piping For Sludge (m) with average multiplication factor 1% sludge or below = water										0.00	0.02	0.08	0.18	0.31	0.46	0.65	0.86	1.10	1.37	1.67	1.99	2.34	2.71	3.11	3.54	3.98	4.46	4.95	5.48					

HEAD LOSS FOR PIPE FITTINGS [for Metric Units h_f=K{(v²/2g)}], based on Table B-6 of "Pumping Station Design", Second Edition, Butterworth Heinemann.

	Nominal Pipe Size (mm)	Pipe Size- ID (m)	Increaser Smaller ID (m)	Pipe Fitting		K-Factor	K Correction Factor	HEAD LOSS (M) THROUGH FITTINGS																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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System Curve Data

Cumulative data from the TDH Pump curves. This data is used to generate the System Curves for 3 MOE conditions

Pump Flow (L/s)	0	15	30	45	60	75	90	105	120	135	150	165	180	195	210	225	240	255	270	285
Condition A, 2 Pump	13.85	13.89	13.99	14.15	14.37	14.65	14.98	15.36	15.80	16.29	16.83	17.42	18.06	18.76	19.50	20.30	21.14	22.03	22.98	23.97
Condition B, 2 Pump	13.40	13.43	13.53	13.67	13.87	14.12	14.42	14.77	15.17	15.62	16.11	16.65	17.24	17.88	18.56	19.28	20.05	20.87	21.74	22.64
Condition C, 2 Pump	12.95	12.98	13.07	13.20	13.38	13.61	13.89	14.21	14.58	14.99	15.45	15.95	16.49	17.08	17.71	18.38	19.09	19.85	20.65	21.49
Condition B, 1 Pump	13.40	13.45	13.59	13.80	14.10	14.48	14.93	15.46	16.06	16.74	17.49	18.31								
Overflow Condition, 2 Pump	0.70	0.73	0.83	0.97	1.17	1.42	1.72	2.07	2.47	2.92	3.41	3.95	4.54	5.18	5.86	6.58	7.35	8.17	9.04	9.94

Flow Demand Data (For Graph)

Dieppe 20 Year Peak Flows

Maximum flow through for Head

150.0000

0

150.0000

16.83

150.0000

16.83

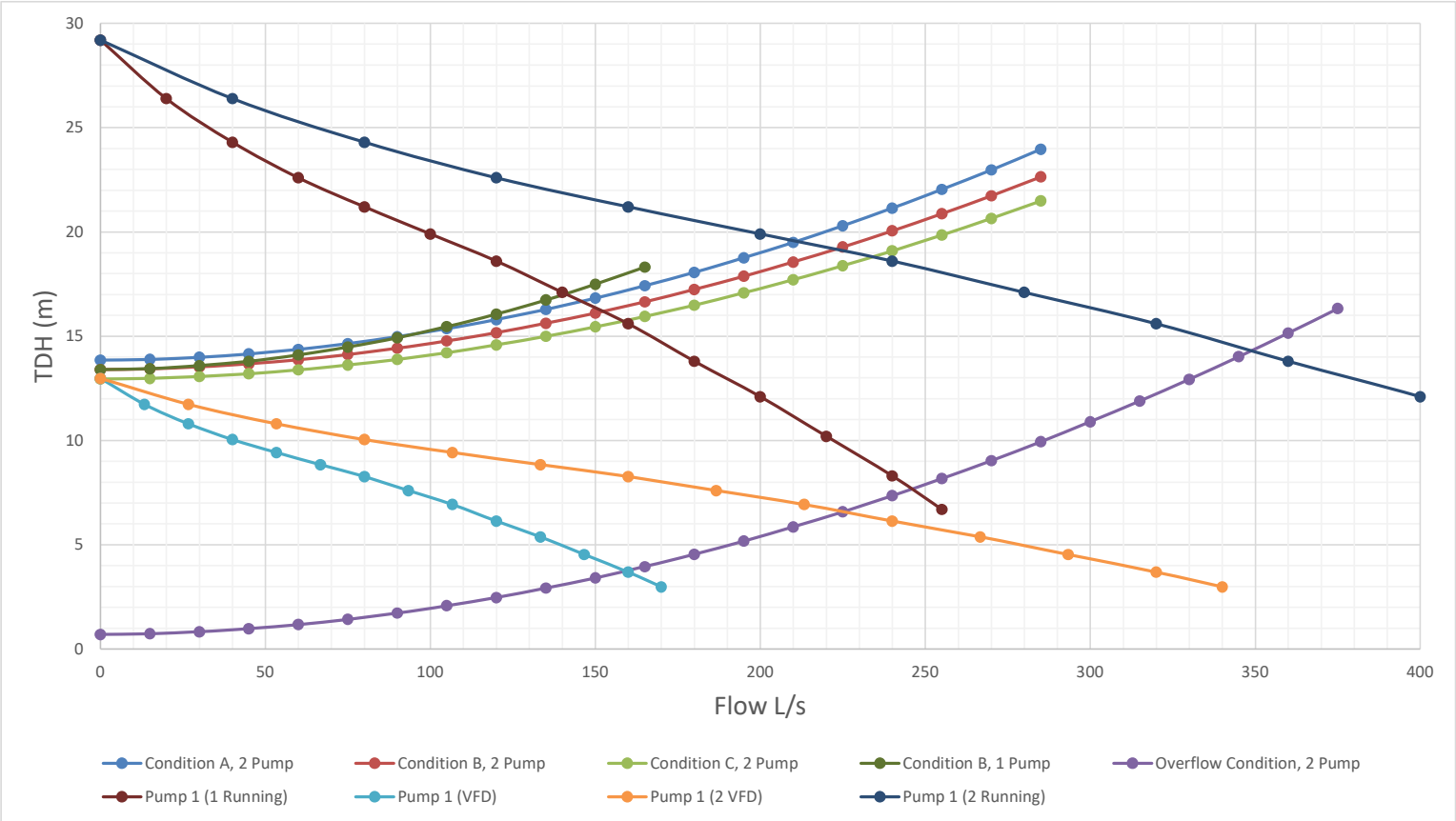
Pump Curve Data

Pump 1 (1 Running)		Pump 1 (VFD)		Pump 1 (2 Running)		Pump 1 (2 VFD)	
Flow	Head	Flow	Head	Flow	Head	Flow	Head
0	29.2	0	12.98	0	29.20	0	12.98
20	26.4	13.33	11.73	40	26.40	27	11.73
40	24.3	26.67	10.80	80	24.30	53	10.80
60	22.6	40.00	10.04	120	22.60	80	10.04
80	21.2	53.33	9.42	160	21.20	107	9.42
100	19.9	66.67	8.84	200	19.90	133	8.84
120	18.6	80.00	8.27	240	18.60	160	8.27
140	17.1	93.33	7.60	280	17.10	187	7.60
160	15.6	106.67	6.93	320	15.60	213	6.93
180	13.8	120.00	6.13	360	13.80	240	6.13
200	12.1	133.33	5.38	400	12.10	267	5.38
220	10.2	146.67	4.53	440	10.20	293	4.53
240	8.3	160.00	3.69	480	8.30	320	3.69
255	6.7	170.00	2.98	510	6.70	340	2.98

Flygt NT 3202 MT3~641 354 mm

Hz

40



NT 3202 MT 3~ 641

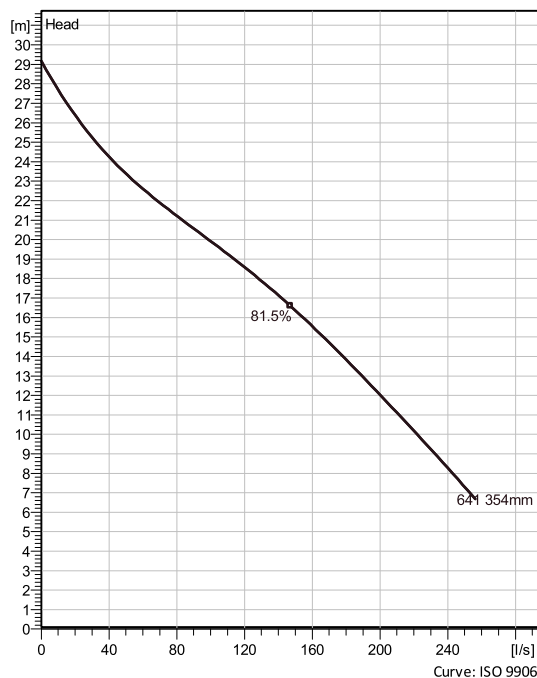
Patented self cleaning semi-open channel impeller, ideal for pumping in waste water applications. Modular based design with high adaptation grade.



Technical specification



Curves according to: Water, pure Water, pure [100%], 4 °C, 1 kg/dm³, 1.569 mm²/s



Nominal (mean) data shown. Under- and over-performance from this data should be expected due to standard manufacturing tolerances.
Please consult your local Flygt representative for performance guarantees.

Configuration

Motor number N3202.800 30-37-6IE-D IE3 44hp	Installation type T - Vertical Permanent, Dry
Impeller diameter 354 mm	Discharge diameter 200 mm

Pump information

Impeller diameter 354 mm
Discharge diameter 200 mm
Inlet diameter 250 mm
Maximum operating speed 1185 1/min
Number of blades 2
Max. fluid temperature 40 °C

Material

Impeller Grey cast iron

Project Xylect-21386358
Block 0

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NT 3202 MT 3~ 641

Technical specification



Motor - General

Motor number N3202.800 30-37-6IE-D IE3 44hp	Phases 3~	Rated speed 1185 1/min	Rated power 33 kW
ATEX approved No	Number of poles 6	Rated current 44 A	Stator variant 3
Frequency 60 Hz	Rated voltage 600 V	Insulation class H	Type of Duty S1
Version code 800			

Motor - Technical

Power factor - 1/1 Load 0.76	Motor efficiency - 1/1 Load 94.5 %	Total moment of inertia 0.629 kg m ²	Starts per hour max. 30
Power factor - 3/4 Load 0.68	Motor efficiency - 3/4 Load 94.8 %	Starting current, direct starting 325 A	
Power factor - 1/2 Load 0.55	Motor efficiency - 1/2 Load 94.3 %	Starting current, star-delta 108 A	

Project	Xylect-21386358
Block	0

Created by	
Created on	11/3/2023
Last update	11/3/2023

NT 3202 MT 3~ 641

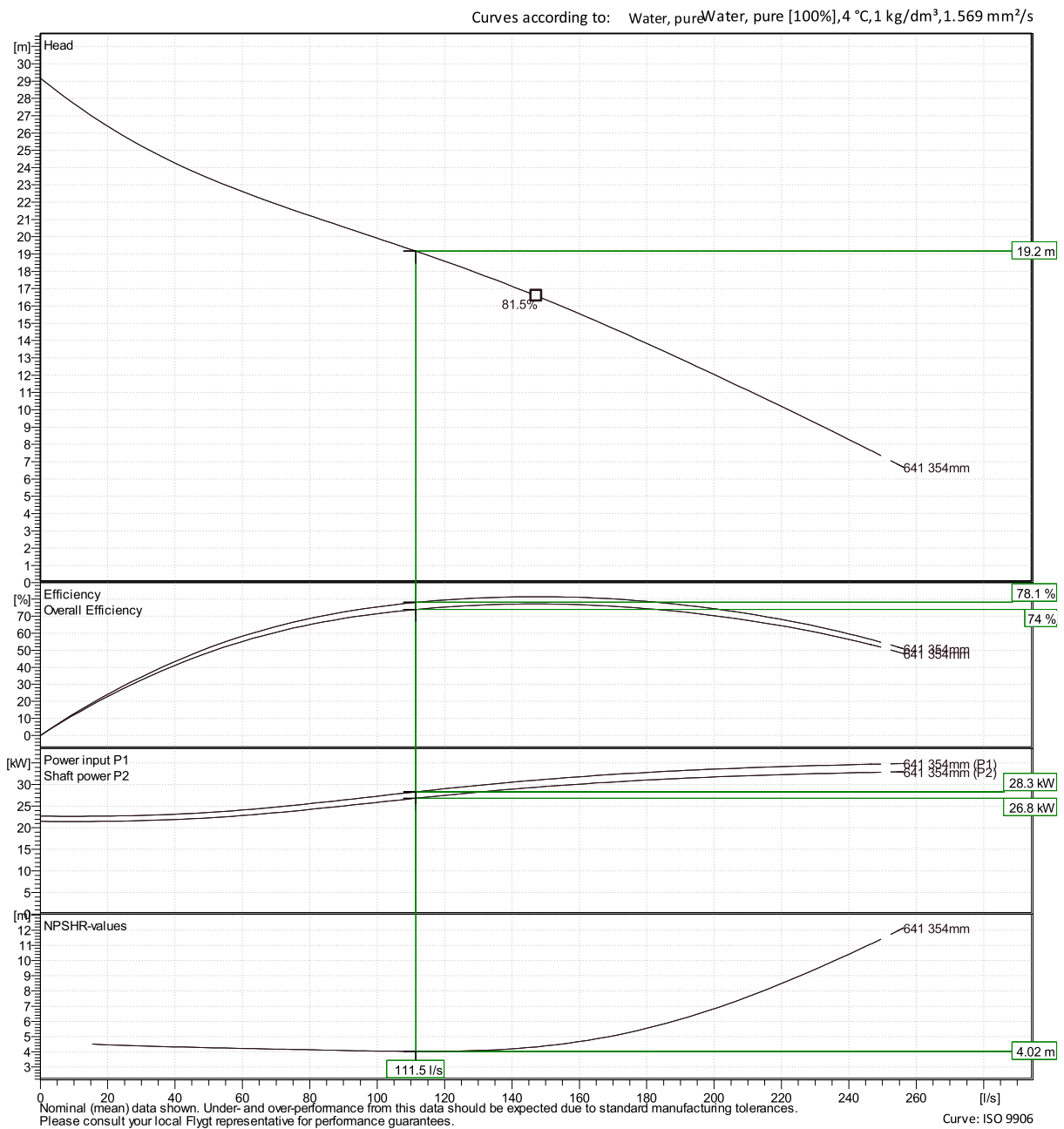
Performance curve



Duty point

Flow
111 l/s

Head
19.2 m



Xylect-21386358

0

Created on

11/3/2023

Last update

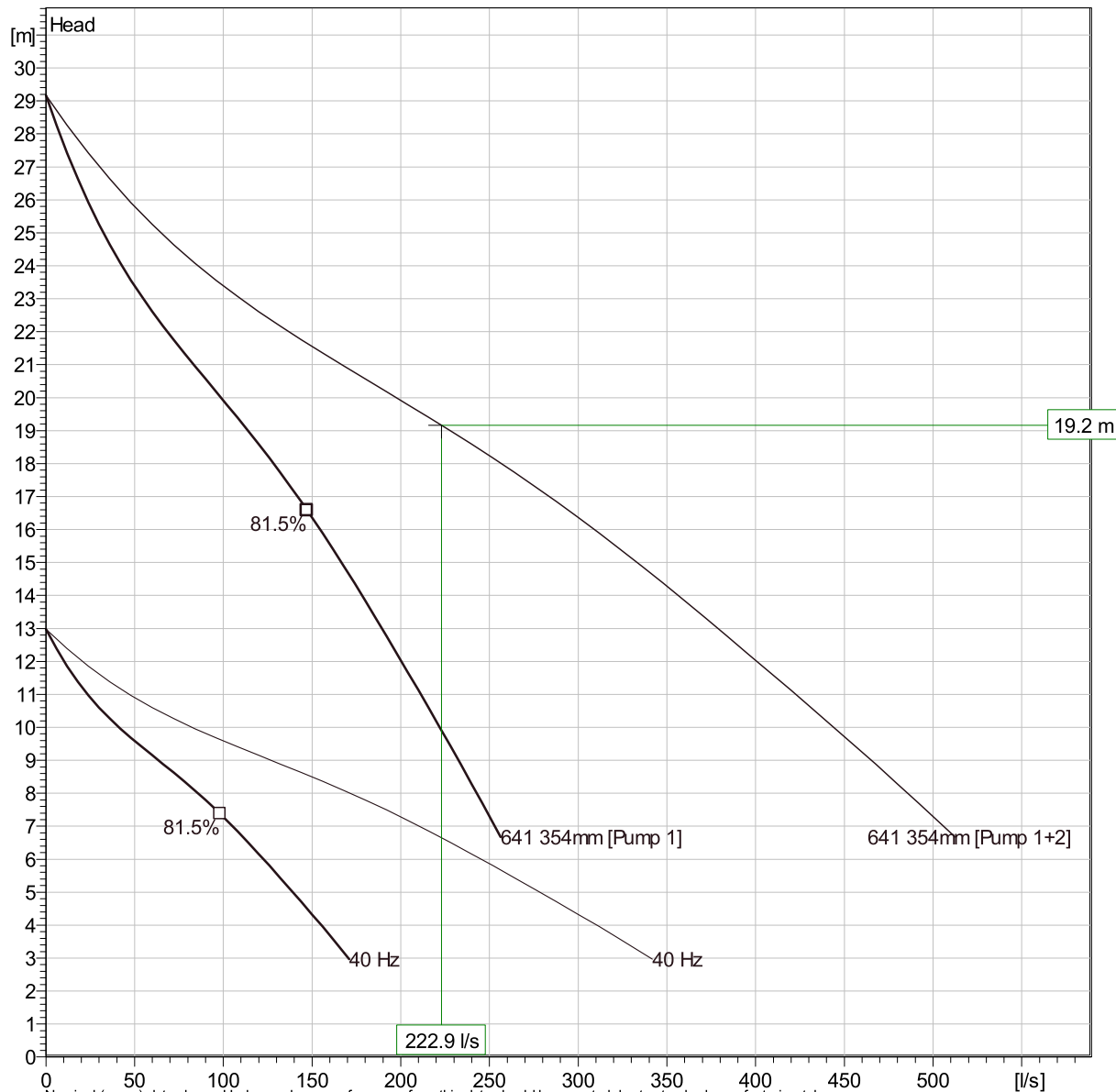
11/3/2023

NT 3202 MT 3~ 641

Duty Analysis



Curves according to: Water, pure [100%] ; 4°C; 1kg/dm³; 1.569mm²/s



Nominal (mean) data shown. Under- and over-performance from this data should be expected due to standard manufacturing tolerances.
Please consult your local Flygt representative for performance guarantees.

Operating characteristics

Pumps / Systems	Flow l/s	Head m	Shaft power kW	Flow l/s	Head m	Shaft power kW	Hydr.eff.	Spec. Energy kWh/l	NPSHre m
2 / 3	172	14.5	30.7	345	14.5	61.4	79.8 %	5.23E-5	5.16
1 / 3	246	7.71	32.8	246	7.71	32.8	56.7 %	3.92E-5	11
2 / 2	96.5	20.1	25.6	193	20.1	51.2	74.5 %	7.77E-5	4.06

Project

Block Xylect-21386358

Created by

Created on 11/3/2023

Last update

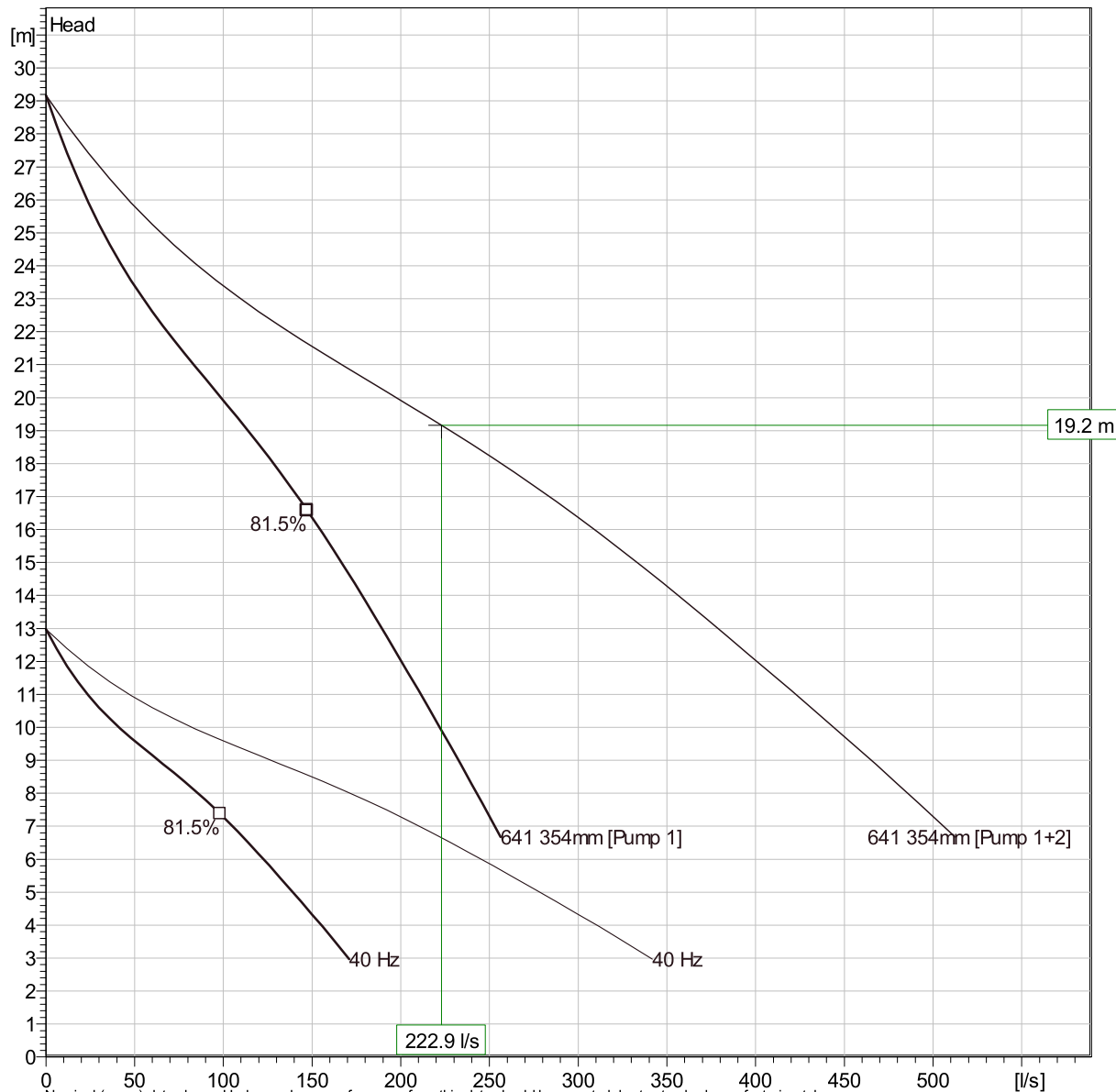
11/3/2023

NT 3202 MT 3~ 641

Duty Analysis



Curves according to: Water, pure [100%] ; 4°C; 1kg/dm³; 1.569mm²/s



Nominal (mean) data shown. Under- and over-performance from this data should be expected due to standard manufacturing tolerances.
Please consult your local Flygt representative for performance guarantees.

Operating characteristics

Pumps / Systems	Flow l/s	Head m	Shaft power kW	Flow l/s	Head m	Shaft power kW	Hydr.eff.	Spec. Energy kWh/l	NPSHre m
1 / 2	142	17	29	142	17	29	81.4 %	6.02E-5	4.22
2 / 1	111	19.2	26.8	223	19.2	53.7	78.1 %	7.06E-5	4.02
1 / 1	153	16.1	29.7	153	16.1	29.7	81.4 %	5.7E-5	4.46

Project

Block Xylect-21386358

Created by

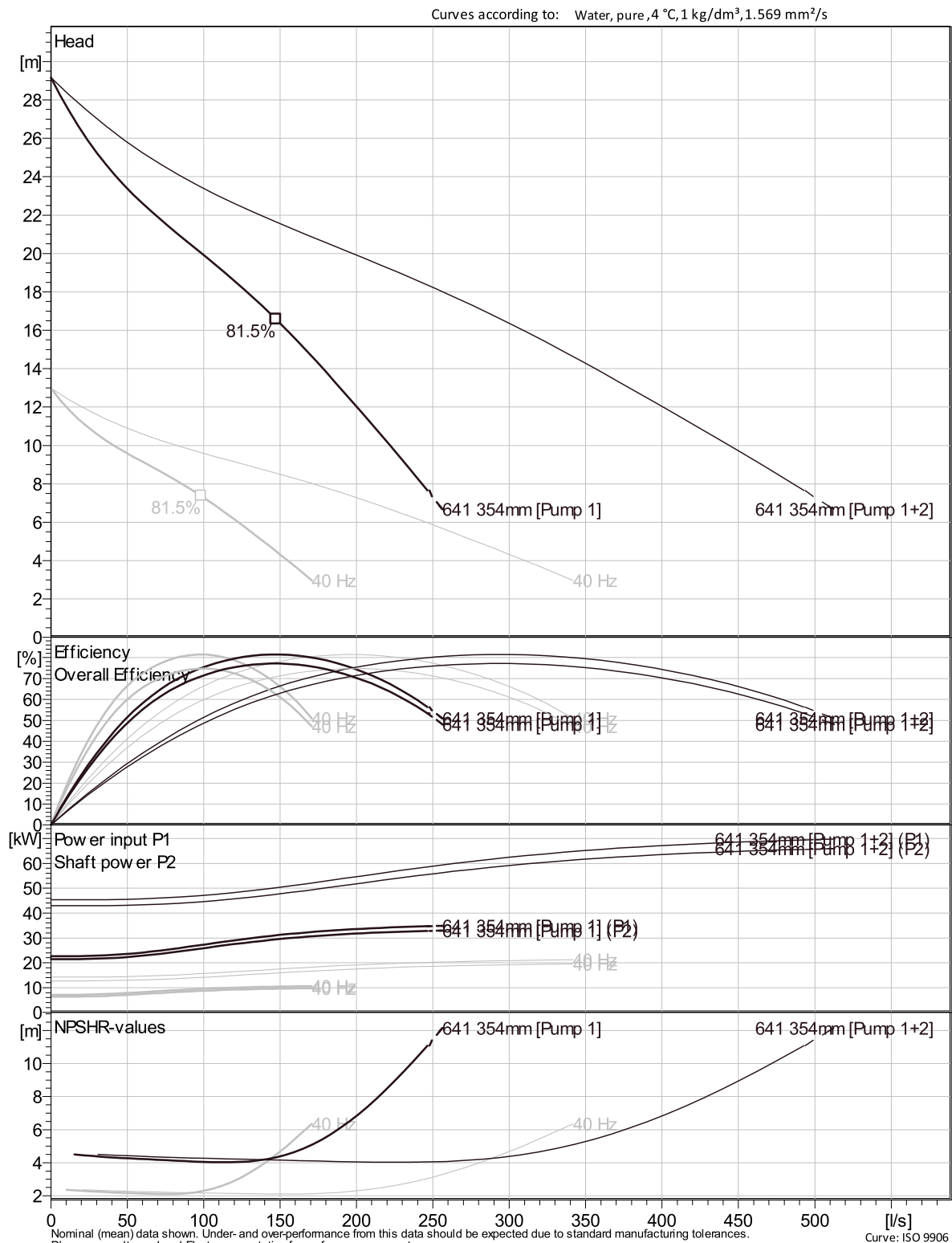
Created on 11/3/2023

Last update

11/3/2023

NT 3202 MT 3~ 641

VFD Curve

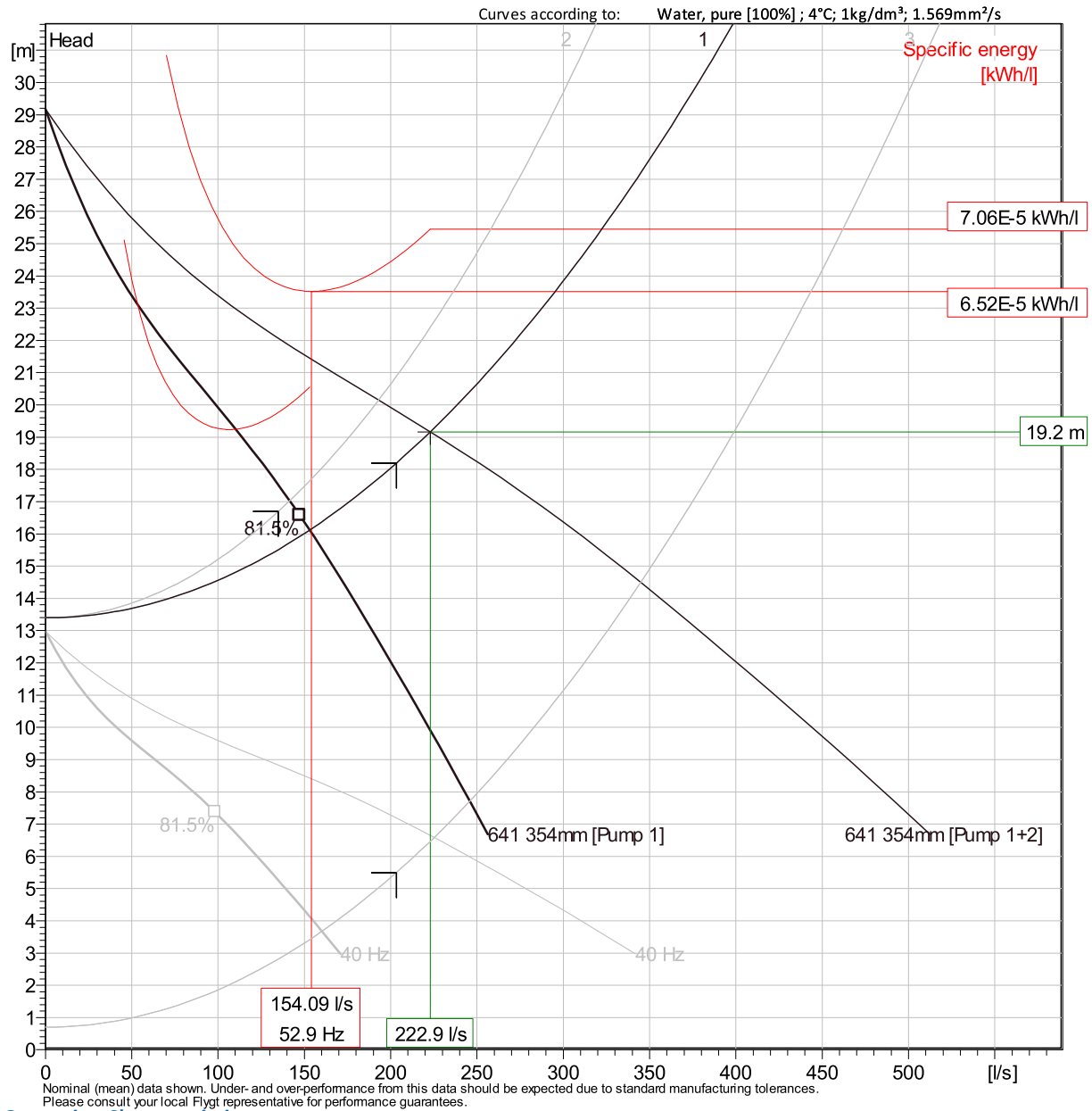


Project Xylect-21386358
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Created on 11/3/2023 Last update 11/3/2023

NT 3202 MT 3~ 641

VFD Analysis



Operating Characteristics

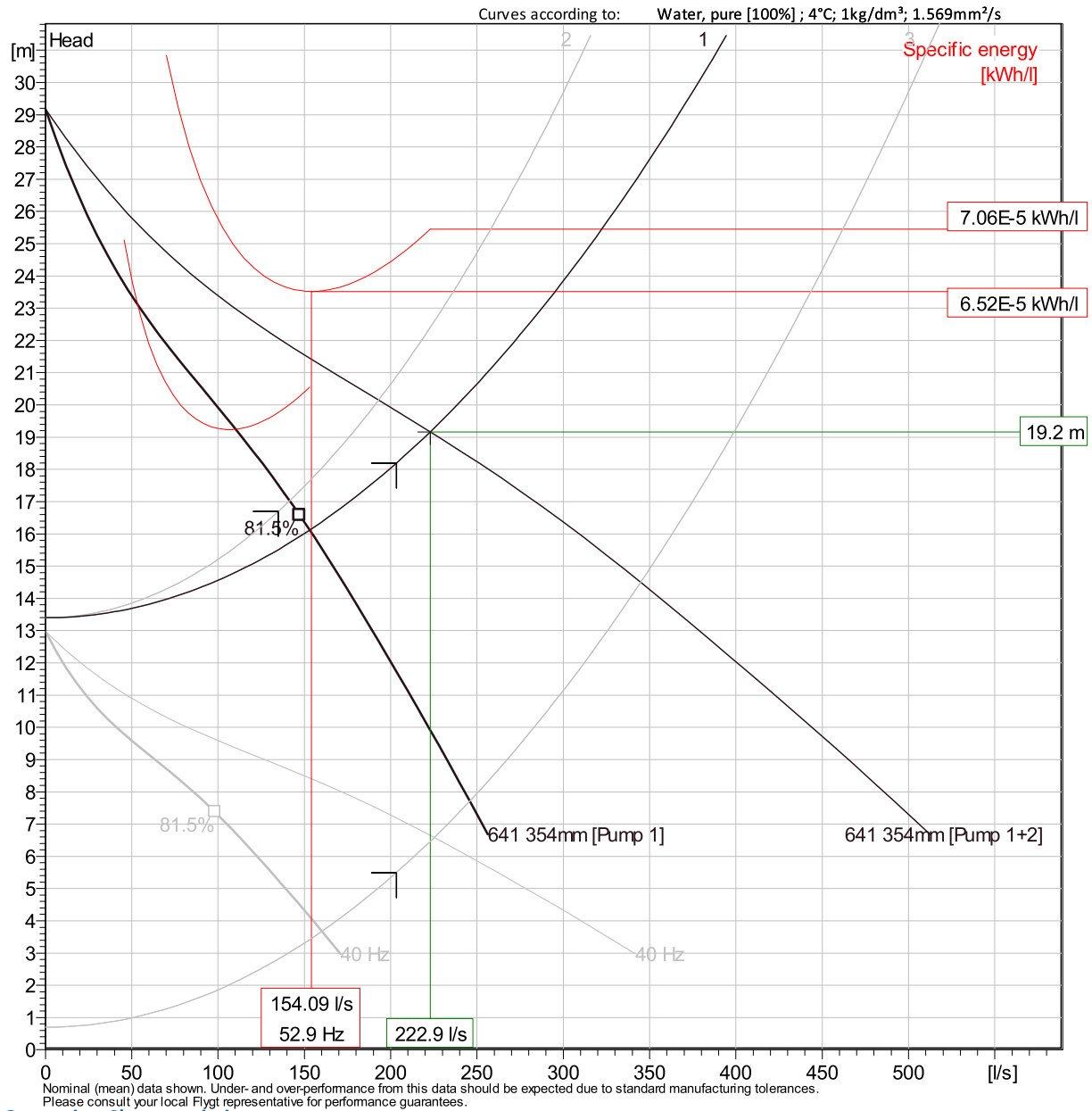
Pumps / Systems	Frequency	Flow	Head	Shaft power	Flow	Head	Shaft power	Hydr. eff.	Specific energy	NPSHre
		l/s	m	kW	l/s	m	kW		kWh/l	m
2 / 3	60 Hz	172	14.5	30.7	345	14.5	61.4	79.8 %	5.23E-5	5.16
2 / 3	40 Hz	113	6.58	9.05	225	6.58	18.1	80.3 %	2.43E-5	2.61
1 / 3	60 Hz	246	7.71	32.8	246	7.71	32.8	56.7 %	3.92E-5	11
1 / 3	40 Hz	160	3.67	9.69	160	3.67	9.69	59.6 %	1.82E-5	5.45

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Block 0

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Created on 11/3/2023
Last update 11/3/2023

NT 3202 MT 3~ 641

VFD Analysis



Operating Characteristics

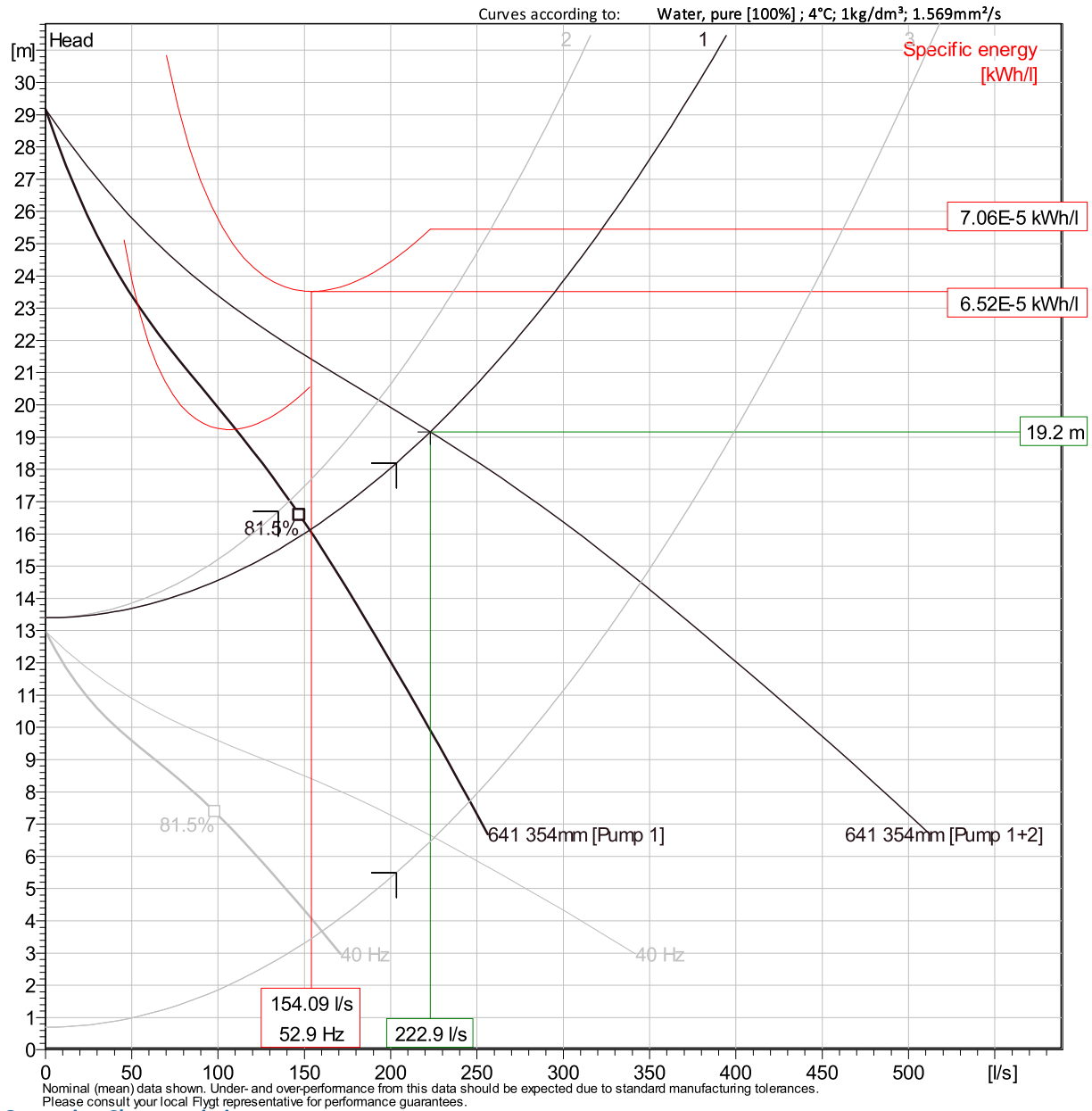
Pumps / Systems	Frequency	Flow l/s	Head m	Shaft power kW	Flow l/s	Head m	Shaft power kW	Hydr. eff.	Specific energy kWh/l	NPSHr m
2 / 2	60 Hz	96.5	20.1	25.6	193	20.1	51.2	74.5 %	7.77E-5	4.06
2 / 2	40 Hz									
1 / 2	60 Hz	142	17	29	142	17	29	81.4 %	6.02E-5	4.22
1 / 2	40 Hz									

Project Xylect-21386358
Block 0

Created by
Created on 11/3/2023
Last update 11/3/2023

NT 3202 MT 3~ 641

VFD Analysis



Operating Characteristics

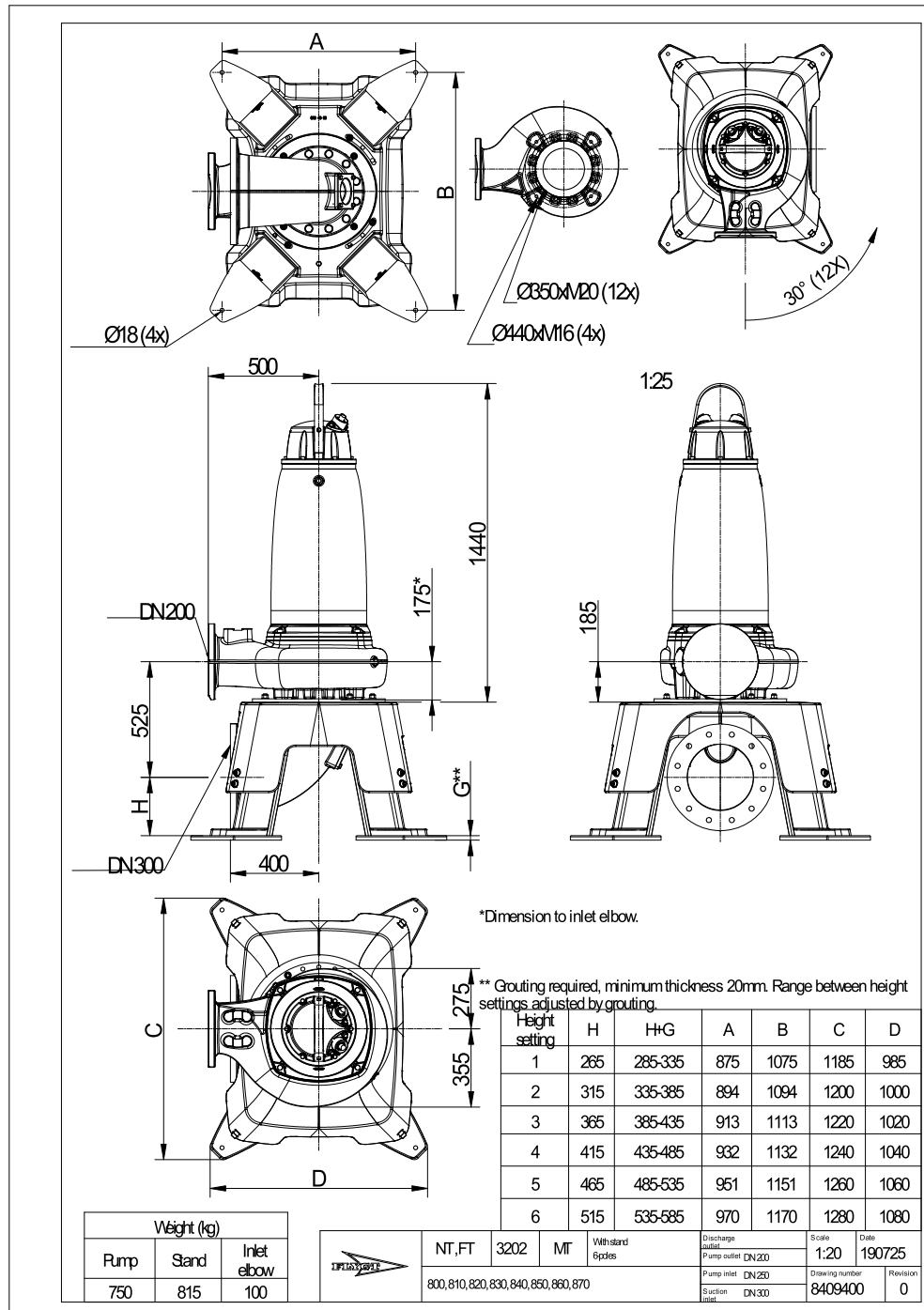
Pumps / Systems	Frequency	Flow	Head	Shaft power	Flow	Head	Shaft power	Hydr. eff.	Specific energy	NPSHre
		l/s	m	kW	l/s	m	kW		kWh/l	m
2 / 1	60 Hz	111	19.2	26.8	223	19.2	53.7	78.1 %	7.06E-5	4.02
2 / 1	40 Hz									
1 / 1	60 Hz	153	16.1	29.7	153	16.1	29.7	81.4 %	5.7E-5	4.46
1 / 1	40 Hz									

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Created on 11/3/2023
Last update 11/3/2023

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Dimensional drawing



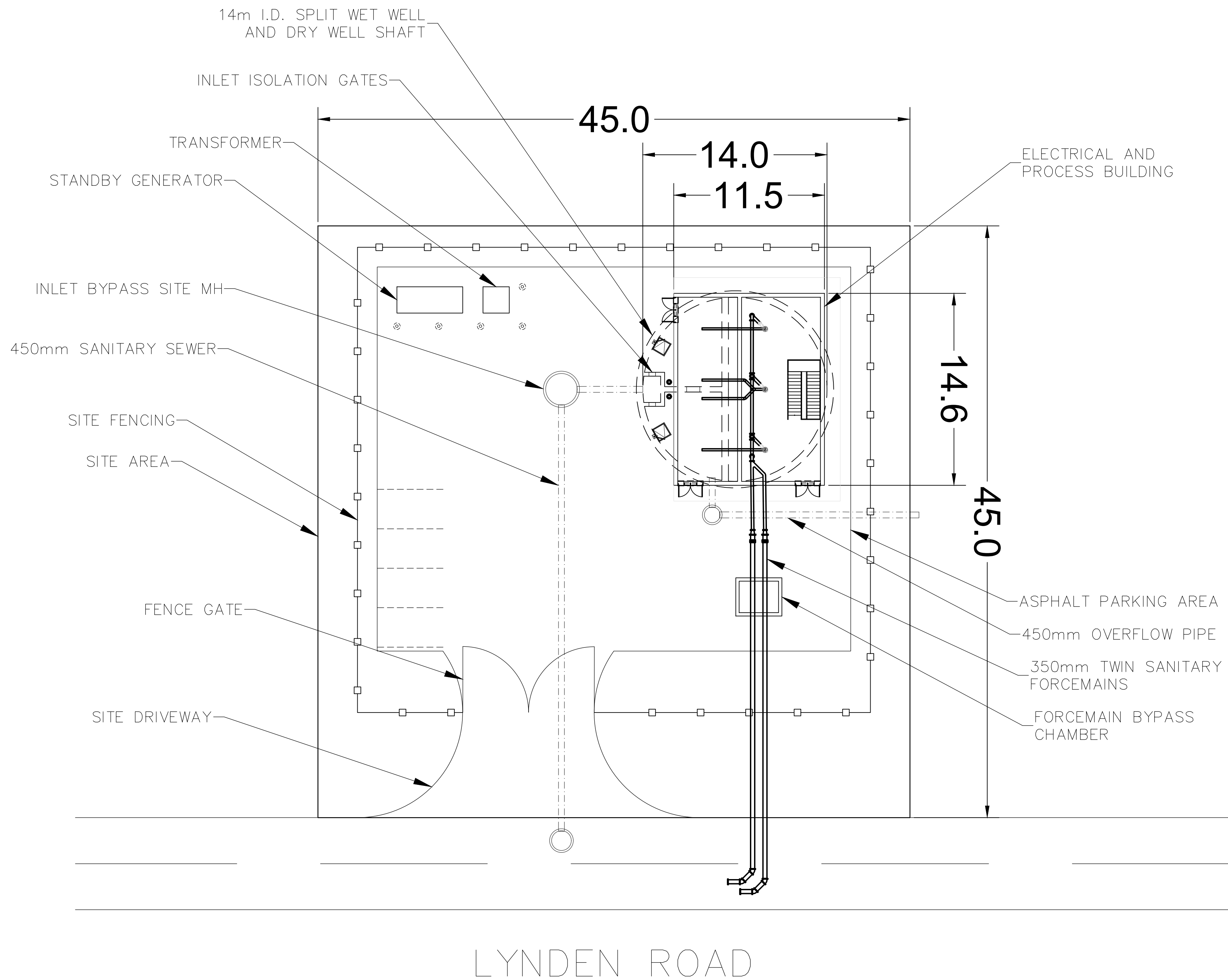
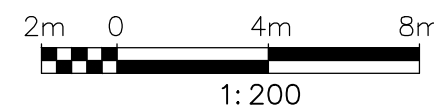
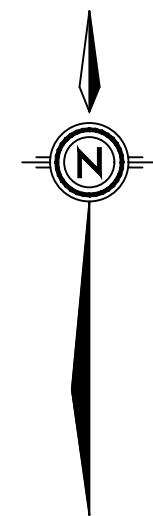
Project Xylect-21386358
Block 0

Created by
Created on 11/3/2023 Last update 11/3/2023

APPENDIX 4

Conceptual Site Plan Drawing

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Plot: 2023-11-07 5:47 PM
###



A	2023.11.07	ET	ISSUED FOR CONCEPTUAL DESIGN
NO.	DATE	NAME	REVISIONS

DESIGNED
ET
DRAFTED
AC
CHECKED
ET
APPROVED
ET



SCALE
BAR IS 25 mm ON ORIGINAL DRAWING
0 mm  25 mm
IF NOT 25mm ON THIS SHEET, ADJUST SCALES ACCORDINGLY.



R.V. Anderson Associates Limited
engineering • environment • infrastructure

RVA Project No.
226497

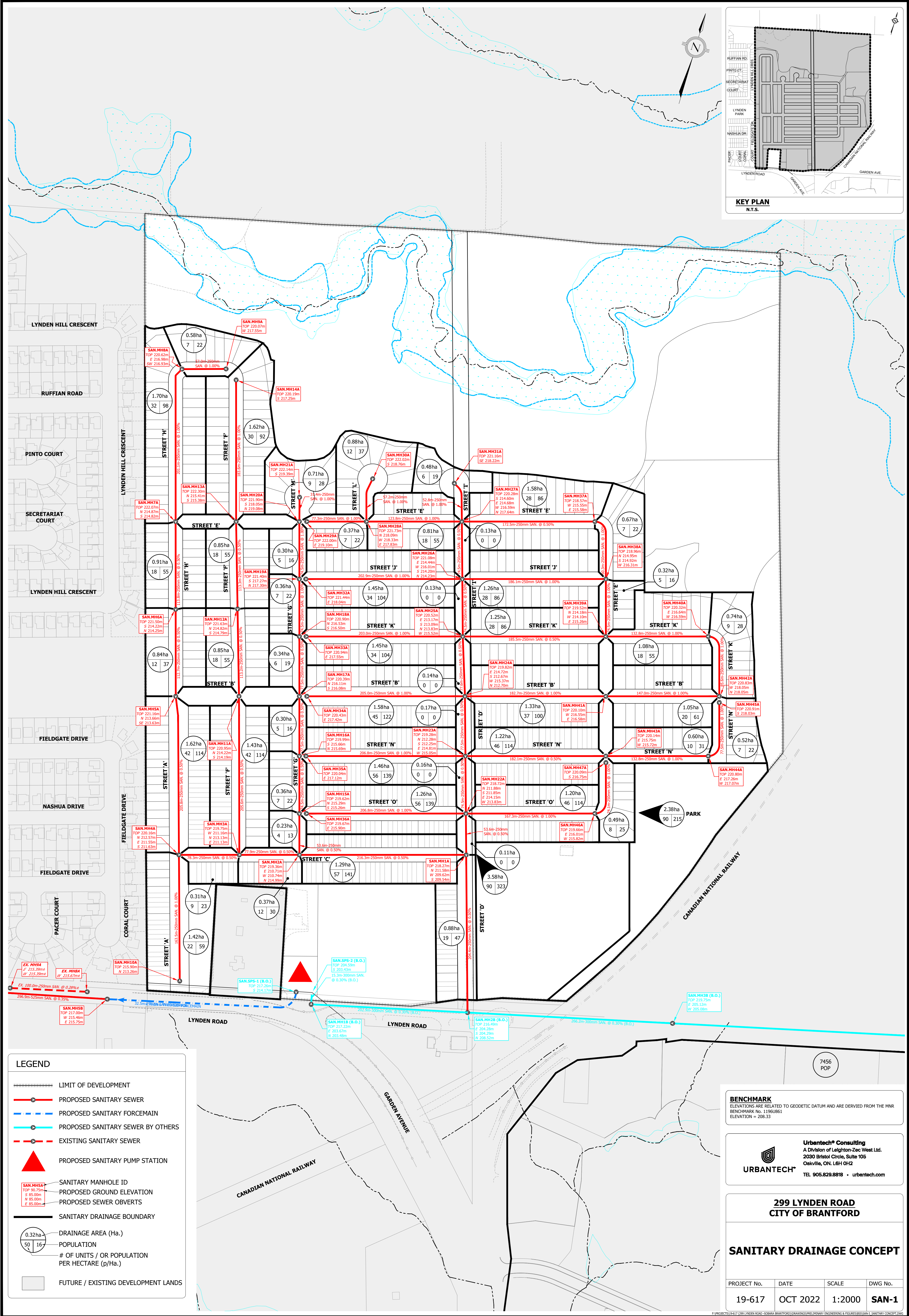
LYNDEN GARDEN BLOCK PS

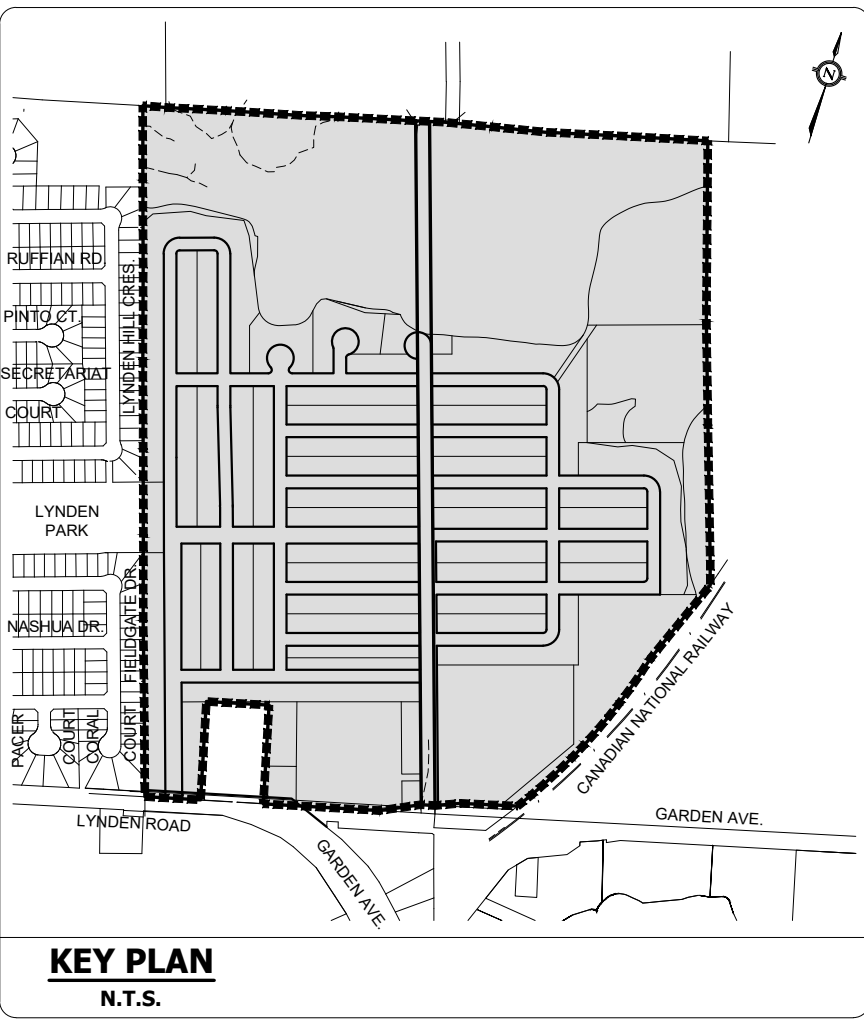
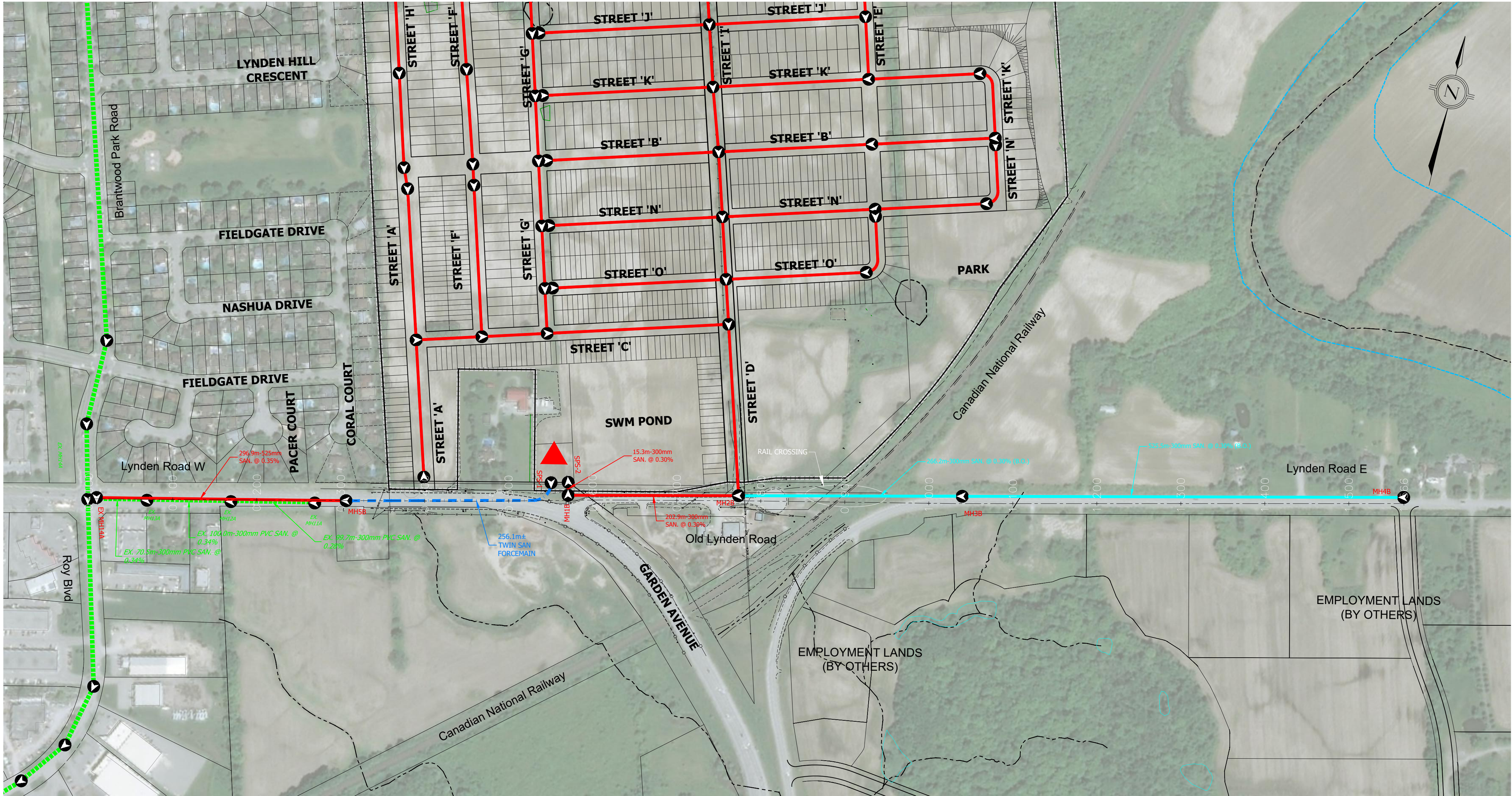
CIVIL
CONCEPTUAL
GENERAL SITE PLAN

CONTRACT NUMBER XX-XXXX-XX
DRAWING NUMBER XXX
SHEET NUMBER X OF X

APPENDIX 5

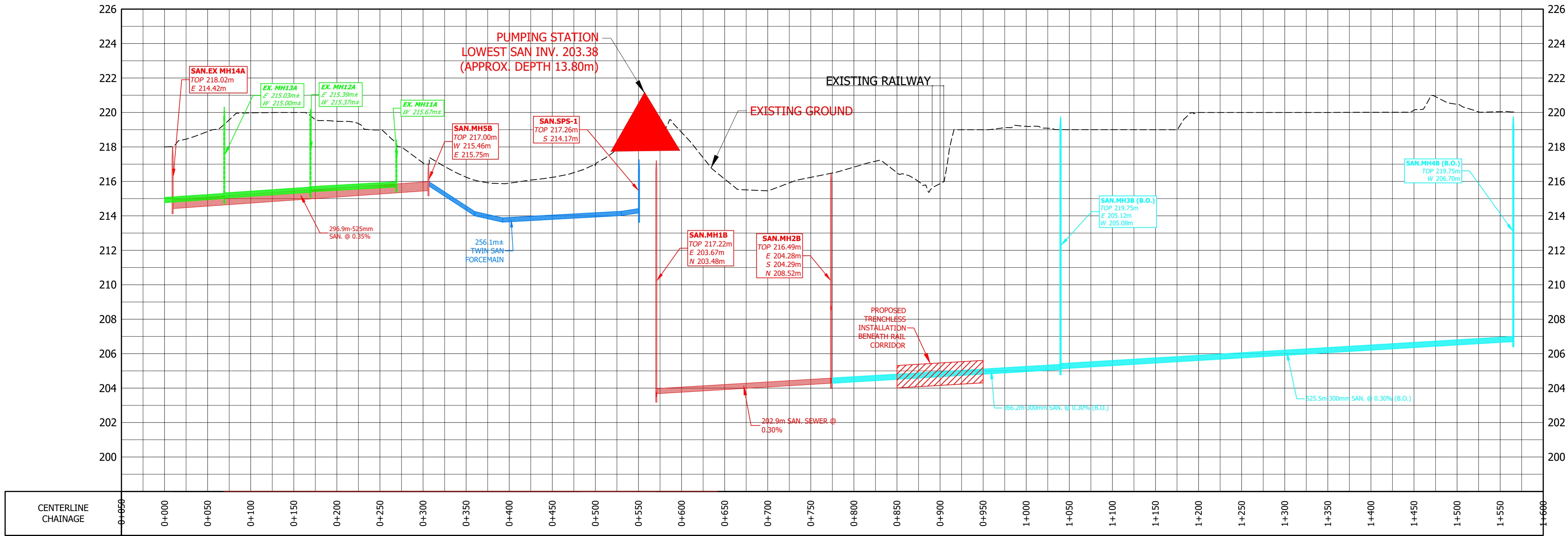
Lynden Garden Block Subdivision Design Drawings





LEGEND

- EXISTING CONTOURS
- EXISTING SANITARY SEWER
- GRAVITY SANITARY SEWER
- GRAVITY SANITARY SEWER BY OTHERS
- PUMPING STATION
- TWIN FORCEMAIN LAYOUT



BENCHMARK
ELEVATIONS ARE RELATED TO GEODETIC DATUM AND ARE DERIVED FROM THE MNR
BENCHMARK No. 1196J861
ELEVATION = 208.33

URBANTECH
Urbantech Consulting
A Division of Leighton-Zec West Ltd.
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**299 LYNDEN ROAD
CITY OF BRANTFORD**

**EAST EXPANSION LANDS
PUMPING STATION**

PROJECT No.	DATE	SCALE	DWG No.
19-617	APR. 2022	H: 1:3,000 V: 1:150	SAN-EXT